# Techniques for Generating a "Real World" Ephemeris

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Prepared by J. A. PEARSON, R. W. BRUCE, and R. C. GORE Electronics Division

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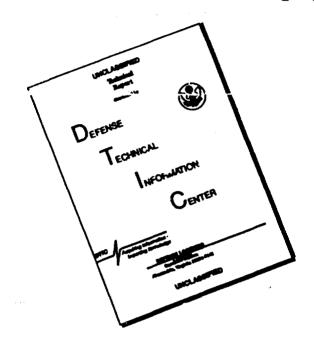


Prepared for SPACE AND MISSILE SYSTEMS ORGANIZATION
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Security Classification

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Security classification of title, body of abstract and index	INTROL DATA - R 8		the overall report is classified;
1 ORIGINATING ACTIVITY (Corporate author) The Aerospace Corporation			Unclassified
El Segundo, California		2 b GROU	
3. REPORT TITLE		<del></del>	
TECHNIQUES FOR GENERATING A	'REAL WORLD	" EPHI	EMERIS
4 DESCRIPTIVE NOTES (Type of report and inclusive dates)			
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5 AUTHOR(S) (First name, middle initial, last name)			
J.A. Pearson, R. W. Bruce, and R.	C. Gore		
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6 REPORT DATE	78 TOTAL .U. OF PA	G.E.S.	76 NO. OF REFS
71 JUL Ø1	72	G E 3	5
BE CONTRACT OR GRANT NO.	9 ORIGINATOR'S RE	PORT NUM	
F04701-71-C-0172	TR-0172(2311	.)-4	
b PROJECT NO.			
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13. ABSTRACT	<del></del>		
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DD FORM 1473

UNCLASSIFIED

Security Classification

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Security Classification

14	KEY WORDS
Ephemeris Generation Atmosphere Modeling Geopotential Modeling Models Drag Trajectories Real World	
	Distribution Statement (Continued)
	Abstract (Continued)

UNCLASSIFIED

Security Classification

Air Force Report No. SAMSO-TR-71-237

Aerospace Report No. TR-0172(2311)-4

# TECHNIQUES FOR GENERATING A "REAL WORLD" EPHEMERIS

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SPACE AND MISSILE SYSTEMS ORGANIZATION
AIR FORCE SYSTEMS COMMAND
LOS ANGELES AIR FORCE STATION
Los Angeles, California

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#### FOREWORD

This report is published by The Aerospace Corporation, El Segundo, California, under Air Force Contract No. F04701-71-C-0172. This report, which documents research carried out from 1 January 1971 through 1 January 1972, was submitted for review and approval on 29 June 1971 to Herbert M. Briesacher, Maj, USAF.

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Publication of this report does not constitute Air Force approval of the report's findings or conclusions. It is published only for the exchange and stimulation of ideas.

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#### ABSTRACT

This report documents the procedure for generating a "real world" ephemeris tape to be used by The Aerospace Corporation and selected contractors in Phase 0 of the Autonomous Navigation System (ANS) contract.

A "real world" geopotential model was developed by modifying a state-of-the-art reference geopotential, using Kaula's degree variances as a guide.

To obtain "real world" atmosphere data, the acceleration profile experienced by the first in a recent series of low altitude satellites to have an on-board low-g accelerometer was suitably scaled. The resulting ephemeris is displayed and subjected to various consistency tests.

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#### SECTION I

#### INTRODUCTION

A "real world" ephemeris tape has been generated for use by The Aerospace Corporation and selected contractors in Phase 0 of the Autonomous Navigation System (ANS) contract. This ephemeris is based on an analytic geopotential force model and an accelerometer data tape (in lieu of an atmosphere model).

To serve as a reference and a standard for comparison, a "model" ephemeris was also generated. This model ephemeris employed the same initial conditions that were to be used in the "real world" ephemeris and used force models that are representative of the state of the art.

Independent of the model ephemeris generation, a geopotential model which simulates the real world was developed. To represent the atmosphere, a span of accelerometer data was taken from an actual satellite flight whose orbit was quite similar to that chosen for the reference. These accelerations were scaled to meet certain criteria to make them suitable for use as a real world atmosphere representation. The detailed development of these models is described in the following sections.

Comparisons between the model and real world ephemerides were performed to ensure that the real world case satisfied certain consistency tests.

Figure 1-1 shows diagrammatically the tasks described above. The work on each task is documented in the section noted parenthetically within the box describing the task.

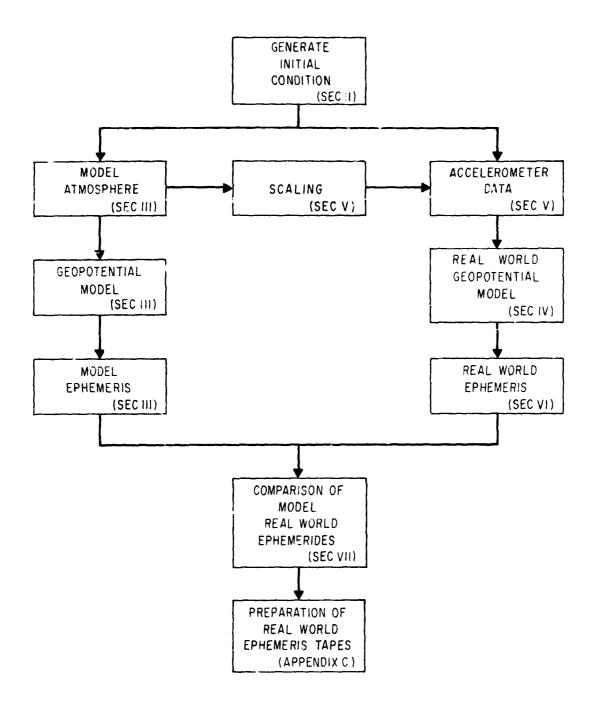


Figure I-1. Task Diagram of SNS Ephemeris Generation

#### SECTION II

#### INITIAL CONDITIONS

The low altitude reference orbit for the ANS has initial perigee occurring within one-half hour of local noon at approximately 45°N latitude. The initial apogee altitude was 200 n mi and perigee altitude was 80 n mi above a spherical earth; its period was about 89.7 min.

Epoch time for this orbit was chosen as 2230 GMT on 29 February 1980. The initial conditions are shown in Table II-1 in four coordinate representations. These are conditions at an ascending node for an orbit having the previously described characteristics.

The first set is an earth-centered inertial (ECI) set which has as its reference plane the true equator at epoch and as its reference direction the mean equinox at 0 hr GMT of the date of epoch.

The second set is an inertial spherical coordinate set having a and b as the right ascension (measured from the X axis, positive eastward) and geocentric latitude (declination) of the vehicle;  $\beta$  is the angle between the velocity vector and the geocentric vertical (the vertical flight path angle); Az is the azimuth of the velocity vector from true north, measured eastward on a plane normal to the geocentric vertical; and R and V are the respective magnitudes of the position and velocity vectors.

The third set is an earth-fixed spherical coordinate set having  $\lambda$  and  $\phi$  as the geodetic latitude and longitude of the vehicle;  $\gamma$  as the angle between the velocity vector and the geocentric horizontal (the horizontal flight path angle); and Az, R, and V as previously defined.

The fourth set is the classical element set, where a and e are the semimajor axis and eccentricty, respectively; i is the inclination of the orbit plane;  $\Omega$  is the right ascension of the ascending node;  $\omega$  is the argument of perigee, the angle between the direction of perigee, and the line of nodes measured from ascending node to perigee; and  $\tau$  is a reference time indicating the time of last perigee passage in minutes from epoch.

Table II-1. Four Representations of Initial Conditions

	(1) Cartesian (ECI)		(2) Spherical
X	-1.59387494563E±7 ft	α	136.390753744 deg
Y	1.51851714534E+7 ft	δ	1.0E-20 deg
Z	3.84199431557E-15 ft	β	90.7298014230 deg
X	6.16441282935E+3 fps	Az	340 deg
Y	6.00674668844E+3 fps	R	2.20130059195E+7 ft
Z	2.36312409387E+4 fps	V	2.51498815029E +4 fps
	(3) Earth-Fixed Spherical		(4) Classical Elements
\	0 deg	а	2.17763946916E+7 ft
0	360 deg	e	1,67413647743E-2
``	-0.7298014230 deg	i	110 deg
Az	340 deg	Ω	136.390753744 deg
R	2.20130059195E+7 ft	ω	131, 193639651 deg
V	2.51498815029E+4 fps	τ	-57.36926627 min

The Greenwich hour angle at 0 hr GMT of the assumed epoch data is 157.9667413 deg. This value is needed to facilitate transformations among these four representations.

The reference ballistic coefficient ( $C_D^A/W$ ) for this vehicle is 0.02 ft<sup>2</sup>/lb. This value is considered typical of future high drag satellite system configurations.

#### SECTION III

#### "MODEL" EPHEMERIS

The TRACE computer program (Ref. 1 and 2) was utilized in generating the model ephemeris. The initial conditions previously discussed were used to generate an ephemeris for 20 orbits spanning approximately 1-1/4 days.

Force models used in the model ephemeris included a 6th degree and order versica of a Guier 8th degree and order geopotential (Ref. 3), and the Jacchia-Walker-Bruce atmosphere model (Ref. 4). A 90-day mean of the 10.7 cm solar flux  $F_{10}$ , denoted  $\overline{F}_{10}$ , is used as a reference about which the short-term decametric flux is measured. Values of  $F_{10} = \overline{F}_{10} = 220 \text{ w/M}^2/\text{cps}$  were used in the model ephemeris. A value of the planetary magnetic index  $a_P = 20$  was also used. Appendix A contains a series of plots showing the ground trace of this vehicle as a function of time. For reference and for later comparison purposes, Table III-1 gives the times and ECI coordinates of the vehicle at each ascending node.

Table III-1. Nodal Conditions for "Model" Ephemeris

Rev No.	Time of Ascension Nodal Cross (Mo/Day/Yr) (Hr/Min/Sec)	Position (ECI) XYZ (ft)	Velocity (ECI) XŸŻ (fps)
0	2/29/80 22/30/0.00	-1.59387495E+7 1.51831715E+7 3.84199432E-15	6.16441283E+3 6.00674669E+3 2.36312409E+4
1	2/29/80 23/59/34.88980	-1.59849728E+7 1.51290676E+7 -3.42450058E-4	6.14526310E+3 6.02746746E+3 2.36342563E+4
2	3/1/80 1/29/9.04968	-1.60306694E+7 1.50749261E+7 -1.27921077E-3	6.12582532E+3 6.04818772E+3 2.36374575E+4
3	3/1/80 2/59/42.38501	-1.60763279E+7 1.50203121E+7 -3.93344718E-4	6.10595310E+3 6.06958938E+3 2.36408159E+3
4	3/1/80 4/16/22.60609	-1.61222326E+7 1.49651661E+7 -3.21860488E-4	6.08579606E+3 6.09047463E+3 2.36442966E+4
5	3/1/80 5/57/46.87890	-1.61677347E +7 1.49098307E +7 -1.29691562E-3	6.06616627E+3 6.11094373E+3 2.36478441E+4
6	3/1/80 7/27/18.02516	-1.62126068E+7 1.48546061E+7 -5.61057958E-5	6.04703706E+3 6.13214743E+3 2.3652798E+4
7	3/1/80 8/56/48.31871	-1.62574412E+7 1.47994091E+7 -1.34453140E-3	6.02763290E+3 6.15356280E+3 2.36544996E+4
8	3/1/80 10/26/17.81324	-1.63022491E+7 1.47441290E+7 -4.84307362E-5	6.00814712E+3 6.17471305E+3 2.36575294E+4
9	3/1/80 11/55/46.47345	-1.63468743E+7 1.46889614E+7 -1.26815078E-3	5.98856274E+3 6.19570106E+3 2.36603321E+4

Table III-1. Nodal Conditions for "Model" Ephemeris (Continued)

Rev No.	Time of Ascension Nodal Cross (Mo/Day/Yr) (Hr/Min/Sec)	Position (ECI) XYZ (ft)	Velocity (ECI) XYZ (fps)
10	3/1/80 13/25/14.30215	-1.63916332E+7 1.46338136E+7 -4.18009639E-4	5.96833727E+3 6.21608673E+3 2.36630337E+4
11	3/1/80 14/54/41.38993	-1.64363722E+7 1.45783174E+7 -2.46736766E-4	5.94752069E+3 6.23585677E+3 2.36659569E+4
12	3/1/80 16/24/7.75793	-1.64807430E+7 1.45224105E+7 -1.30417512E-3	5.92644969E+3 6.25589753E+3 2.36690683E+4
13	3/1/80 17/53/33.34407	-1.65248655E+7 1.44662676E+7 -6.31984487E-4	5.90592687E+3 6.27676825E+3 2.36720090E+4
14	3/1/80 12/22/58.06510	-1.65687876E+7 1.44100661E+7 -6.78497093E-5	5.88630149E+3 6.29783075E+3 2.36747293E+4
15	3/1/80 20/52/21.87667	-1.66124592E+7 1.43537098E+7 -3.22734601E-4	5.86662222E+3 6.31863642E+3 2.36775153E+4
16	3/1/80 22/21/44.78377	-1.66559668E+7 1.42970491E+7 -1.05750460E-3	5.84642459E+3 6.33935065E+3 2.36805229E+4
17	3/1/80 23/51/6.84696	-1.66991600E+7 1.42403605E+7 -1.30152780E-3	5.82597771E+3 6.35945009E+3 2.36837258E+4
18	3/2/80 1/20/28.09812	-1.67418053E+7 1.41837185E+7 -1.32891135E-3	5.80526738E+3 6.37930109E+3 2.36871191E+4
19	3/2/80 2/49/48.44448	-1.67842644E+7 1.41266781E+7 -1.32615034E-3	5.78411142E+3 6.39985957E+3 2.36906835E+4
20	3/2/80 4/19/7.90466	-1.68269602E+7 1.40690575E+7 -1.30997504E-3	5.76259368E+3 6.42012503E+3 2.36943783E+4

#### SECTION IV

#### "REAL WORLD" GEOPOTENTIAL

## A. SIMULATED GRAVITY FIELD GENERATION

For the real world case, the geopotential was expressed as a spherical harmonic expansion of the following form:

$$U = \frac{GM}{r} \left\{ 1 + \sum_{n=2}^{N} \left( \frac{a_e}{r} \right)^n \left[ \overline{C}_{no} \overline{P}_n(\sin \phi) + \sum_{m=1}^{n} \overline{P}_n^{-m} (\sin \phi) (\overline{C}_{nm} \cos m\lambda + \overline{S}_{nm} \sin m\lambda) \right] \right\}$$
(IV-1)

where

U = geopotential

GM = gravitational constant times the mass of the earth

a = equatorial radius of the earth

r = radial distance from the earth's center of mass

 $\phi$  = geocentric latitude

 $\lambda$  = geocentric longitude

 $\overline{P}_{n}^{m}$  = normalized associated Legendre functions

 $\overline{C}_{nm}$ ,  $\overline{S}_{nm}$  = normalized cosine and sine coefficients of the nth degree and mth order

When the gravity field is expressed as such a spherical harmonic expansion, it is completely described by the choice of spherical harmonic coefficients (C, S). This study thus required that a suitable set of C's and S's be selected.

The set of spherical harmonic coefficients used for this study was generated as follows. First, a set of C's and S's was selected from one of the currently available geopotentials published in the literature. Second,

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Table IV-1. Gravity Degree Variances

Degree	Mean of Coefficients with Standard Deviation About the Mean of Reference	Mean of Perturbations with Standard Deviation About Mean X 106
2	-96.6 ± 216.6	0.0015 ± 0.036
3	$0.798 \pm 0.853$	0.0072 ± 0.019
4	$0.154 \pm 0.525$	$0.0123 \pm 0.120$
5	$-0.094 \pm 0.361$	$-0.028 \pm 0.075$
6	$-0.152 \pm 0.216$	$-0.023 \pm 0.054$
7	$0.026 \pm 0.192$	$0.0018 \pm 0.045$
8	$0.026 \pm 0.131$	-0.0069 ± 0.036
9	$0.013 \pm 0.118$	$0.0055 \pm 0.042$
10	$-0.023 \pm 0.095$	$-0.009 \pm 0.035$
11	$-0.036 \pm 0.076$	$0.014 \pm 0.027$
12	$-0.0014 \pm 0.109$	$0.0039 \pm 0.033$
13	$0.015 \pm 0.079$	$0.0083 \pm 0.028$
14	$0.015 \pm 0.081$	$-0.0036 \pm 0.029$
15	$0.0081 \pm 0.063$	$0.003 \pm 0.032$
16	$-0.0151 \pm 0.0685$	-0.0095 ± 0.0278
17	$-0.0032 \pm 0.0539$	$-0.0003 \pm 0.0268$
18	$-0.0043 \pm 0.060$	$0.0006 \pm 0.030$
19	$0.0036 \pm 0.051$	$-0.0022 \pm 0.029$
20	-0.00066 ± 0.025	0.0037 ± 0.022
21	$-0.0020 \pm 0.011$	$0.00052 \pm 0.029$
22	$-0.0011 \pm 0.015$	$0.00012 \pm 0.023$
23	$0.00055 \pm 0.023$	$0.00284 \pm 0.020$
24	$0.0027 \pm 0.010$	$-0.0012 \pm 0.021$

perturbations were then algebraically added to the set of coefficients in a way that left the lower degree features of the field unchanged but introduced increasing amounts of variation with increasing degree. Third, additional coefficients were generated for those terms not provided in the original set to increase the degree of the resulting simulated gravity field to the maximum size permitted by existing software.

Perturbations to the reference field were generated in the following manner: First, a degree variance was chosen for every degree 2 through 24. Table IV-1 shows the degree variance used in generating this field, the values obtained and published by W. M. Kaula (Ref. 5), and the values obtained from the reference set. As can be seen from the table, the degree variances were chosen to introduce very small perturbations in the lower degree field with an increasing variation as upper degree fields were generated, until finally at 19th degree a field would be produced that roughly obeyed the properties reported by Kaula.

For every degree variance of Table IV-1 (column 1), a set of coefficient perturbations,  $\overline{\Delta C}_{nm}$ ,  $\overline{\Delta S}_{nm}$ , was chosen from a random number generator such that the sum of the squares of these coefficients would satisfy the equation

$$\sigma_{n}^{2} = \frac{1}{g_{e}^{2}(n-1)^{2}} \sum_{m=0}^{n} \overline{\Delta C}_{nm}^{2} + \overline{\Delta S}_{nm}^{2}$$
 (IV-2)

where  $\sigma_n^2$  is the degree variance and  $g_e$  is the mean equatorial gravity.

Finally, the coefficients generated by this process were algebraically added to the coefficients of identical degree and order in the reference set, and the result was then used as the final representation of the earth's gravity field.

Using the above method, a field was generated complete to 24th degree and order. This field above 19th degree is, essentially, a random field conforming only to the constraint of Eq. (IV-2). For 19th degree and under, the field is a slightly varied form of the reference field. This can be seen

Table IV-2. Geopotential Coefficient Statistics

Degree	Degree Variance Used in Generating Perturbation (mgal <sup>2</sup> )	Degree Variance Reported by Kaula (Ref. 5)(mgal <sup>2</sup> )	Degree Variance from Reference (mgal <sup>2</sup> )
2	0.005	7.	7.6
3	0.01	44.	33.9
4	1.	30.	20.9
5	i.	10.	21.5
6	1.	24.	20.6
7	1.	3.	18.2
8	1.	23.	13.5
9	2.	22.	15.5
10	2.	15.	14.9
11	2.	18.	15.0
12	3.	7.	33.0
13	3.	15.	23.5
14	4.	23.	30.6
15	6.	22.	23.0
16	6.	6.	34.1
17	6.	12.	24.3
18	9.	19.	36.0
19	10.	10.	30.9
20	7.	7.	8.7
21	14.	14.	1.9
22	10.	10.	4.0
23	9.	9.	11.4
24	11.	11.	2,7

more clearly in Table IV-2, which gives the results of averaging both the reference set and the perturbation set of coefficients over all coefficients of the same degree. The sigma presented in Table IV-2 is the variance of the coefficients of a particular degree about the mean of the coefficients of that same degree. This sigma should not be interpreted as any measure of accuracy of the coefficients but is included to provide some measure of the variation of coefficients of a particular degree.

Table IV-3 presents the final set of coefficients generated for this study. These coefficients should be used with the expression for earth gravity potential given in Eq. (IV-1).

## B. TEST OF SIMULATED GRAVITY FIELD

The field specified by Table IV-3 was tested for its effect upon the nominal orbit. This test was conducted by performing trajectory difference runs with TRACE (see Ref. 1). These difference runs were performed by taking the nominal epoch vector from Table II-1 as an initial condition from which an orbit was obtained by numerical integration of the gravity force model. The same process was then repeated with the perturbed gravity field. The difference between the two orbits at identical times was then resolved into in-track, radial, and cross-track differences.

First, a difference run was made between the Guier n = 6, m = 6 model ("model" geopotential) and the reference model. No atmosphere model was included. The purpose of this run was to establish a baseline for the behavior of a high-degree gravity field. (The Guier 6.6 geopotential uses a value of GM = 1.4076538841E+16 ft<sup>3</sup>/sec<sup>2</sup>, while the reference model has a GM = 1.4076468597E+16 ft<sup>3</sup>/sec<sup>2</sup>.) Figures IV-1a, b, and c show the behavior of the in-track, radial, and cross-track differences. The in-track difference shows a secular growth component of approximately 770 ft/rev together with a periodic component with a maximum excursion of 1500 ft; the radial difference shows a periodic variation with a maximum amplitude of approximately 700 ft; the cross-track difference has a maximum periodic difference of 1300 ft.

Table IV-3. "Real World" Normalized Geopotential Spherical Harmonic Coefficients

z	×	<u>C</u> nm	$\overline{S}_{nm}$	Z	Σ	<del>C</del> nm	S <sub>nm</sub>
20	00	-0.48420E-3	0 0, 269052 E-7	07	00	0.160365E-6 0.192085E-6	, !
05	05	24560E-	-0.13568E-5	0.7	02	259770E	143359E
				07	03	322751E	15450E
03	00	973088E-		0.2	04	32667E-	15535E-
03	01	0.2018835-5	.241731E	07	90	143604E	46266E-
03	05	914645E-	-0.64224E-6	07	90	30176E	0.142523E-6
03	03	732356E-	.139657E	0.2	07	537338E	130910E
04	00	969699	0	08	00	510865E-	0
94	01	61604E	8214	80	01	0.690357E-7	0.106908E-6
04	05	458155E	.605959E	80	05	57280E-	14529E-
94	03	106926E	-0.88255E-7	80	03	12113	-0.98384E-7
04	04	14290E-	.119265E	80	04	33922E-	113135E-
				80	90	78786E-	111078E-
90	00	57458E-		80	90	69232E-	351645E-
92	01	0.986159E-8	. 12524	80	07	0.255853E-7	526569
90	05	728570E	.38968E-	80	80	[-]	948901压-
90	03	41915E-	G)				
90	04	38836E-	.42354E-	60	00	34882E-	0
92	90	364591	.71663E-	60	01	0.255080E-6	0273E
				60	05	320793E	15763E-
90	00	23179E-	0	60	03	16022E-	112325五
90	01	62937E	636E-	60	04	69222E-	44238
90	02	817727E	.39237E-	60	90	402305	521E-
90	03	35955E	.39050E-	60	90	867828E	.25522E
90	04	77257E-	.53799E-	60	20	10928E-	17379
90	90	28345E-	.59325E	60	80	229342豆	17440E-
90	90	796188	068E-	60	60	75E	2

Table IV-3. "Real World" Normalized Geopotential Spherical Harmonic Coefficients (Continued)

z	×	Cnm	Snm	Z	Σ	Ċ <sub>nm</sub>	S <sub>nm</sub>
10	00	75	0	12	90		804353E-
10	01	34867	. 18495	12	07	0.682487E-7	0.789886E-7
10	05	105952E	.706344E	12	80		683604E-
10	03	12594E	.14879E-	12	60	.767180瓦	113637E-
10	04	287391E	.89879E-	12	10		544306E-
10	05	57062E-	.46122E-	12	11	1-1	45799E
10	90	75825E	.16755E-	12	12		0.113739E-7
10	20	326]	-0.62076E-8				
10	80	44120E-	.72350E-	13	00	-0.28961E-7	0
10	60		1	13	01	0.439583E-7	935374E
10	10	123486E	-0.48686E-7	13	05	0.278303E-7	2045
				13	03	0.329141E-7	1806
11	00	67008E-	0	13	04	-0.58186E-7	-0.13199E-7
11	01	77547E-	-0.16652E-6	13	90	0.571087E-7	196769E
11	05	161544	.284179E	13	90	0.383022E-7	2166
11	03	254468	.19559E-	13	20	-0.65082E-8	35740E-
11	04	46298E-	1182	13	80	0.128901E-7	4941
11	0.5	889578	딥	13	60	0.730744E-7	724142E-
11	90	54230E	.818400	13	10	0.333800E-7	130152E-
11	07	664672E	-0.25796E-7	13	11	-0.35917E-8	60160E-1
11	80	48235E-	.482845	13	12	-0.24347E-7	1345
11	60	34852E	23436E	13	13	-0.21248E-7	477E-
11	10	60133E-	-0.54760E-7				
11	77	456	-0.47852E-7	14	00	.15236E-	
				14	01	56378E	ന
12	00	106234E-	0	14	05	166440E	1994
12	01	277775	766575E	14	03		832372-
12	05	25737E-	260E-	14	04	278466	ທ
12	03	267978E	119924E	14	05		8000E-
12	94	-0.31626E-6	32	14	90	. 698756	0.5:2935E-7
12	0.5	81811E-	136E-	14	20		.181216E-

Table IV-3. "Real World" Normalized Geopotential Spherical Harmonic Coefficients (Continued)

Z	M	Čnm	S <sub>nm</sub>	Z	Σ	<del>Č</del> nm	Snm
14		450234E-	10322	16	80	0.86519E-	61993E-
14	60	57675	309E-	16	60	-0.68630E-8	-0.91682E-7
14		902127E-	676386E	16	10	0.94601E-	0.31916E-
14		38411E-	31449E	16	11	.149005E	48102E-
14		580309E-	59799圧-	16	12	.71449E-	26615E-
14		119424E	154636E-	16	13	.23961E-	382743E
14		64765E-	364691	16	4	.245551E	51547E
				j 6	15	.485409E	87422E-
15	00	19870E	0	16	16	.49682E-	142786E
15	01	44962E-	1824				
15	05	13405E-	109952E-	17	00	03E	0
15	03	1399991	70536E-	17	01	.13606E-	28990E
15	04	139909E	541279E	17	05	0	70914E-
15	90	37062E-	10506E-	17	03	.72390E-	101955E
15	90	33136E-	390408E-	17	04	.46689E-	342571E
15	20	470276E	386850E-	17	90	.449471E	129511E
15	08	-0.11108E-8	0.395489E-7	17	90	0134E	10703E
15	60	21101E-	779548E-	17	07	.44882E-	10686E-6
15	10	504202E	518126E-	17	03	19967E-	903700E-
15	11	87591E	942663E-	17	60	440611E	246408E
15	12	12639E-	203138E-	17	10	68775E-	235640E-
15	13	68930E-	52061E-	17	11	25106E-	19014E-
15	44	116997	2938	17	12	249397E	759679E
15	15	45651E-	1453E-	17	13	급	96739E-
				17	14	7956E-1	25362E-
	00	610667E	0	17	. 15	103419	827257
	01	826119E	702307E	17	16	43663E-	34518E-
	05	18393E-	44119E-	17	17	98659E-	6360E-
16	03	0.935763E-7	-0.22311E-8	<u>~</u>	0	0 70240E	c
	40	23344E-	18945E-	0 7	2	0. 176±0U-	100000
	90	631531E	0.90713E-	0 0	5 6	. 410/4E-/ 0/00/E	407642E
	90	80586E-	45799三-	01	400	0.046600E	10/0425-
	10	22932E-	0.60154E-	21 0	200	-0. (1583E-/ 0. 476555E-6	-0.10/41E-6 0.273448E-7
				0.1	* 5	- 1100001T-	-7010017

Table IV-3. "Real World" Normalized Geopotential Spherical Harmonic Coefficients (Continued)

lable	1 V - 5.	Keal World Nor	World Normalized (reopotential Spherical Harmonic	ıaı Spr	erical	Harmonic Coeffic	Coefficients (Continued)
Z	M	$\bar{C}_{nn_1}$	S <sub>nn</sub>	Z	M	$\overline{C}_{nm}$	<u>S</u> nm
18		32811E	<b>三69</b>	19	17	373620E	58626
18		Q.	-0.34436E-7	19	18	)5E-	핑
<del>2</del>	07	54536E-	71969E	19	19	17153E-	542653
18		197630E	194518E-				
18		9	213571E-		00	108785E	0
18		87832E-	2		0.1	33580E	2982E
18		498471E-	56496E-		05	306763E	.40429E-8
18		264072E-	49071E-		03	13322E-	.214574E-
18		230824E	65927E-		04	:579	.296186E-
18	14	198402E-	0.67111E		0.5	6E-	365E
8	15	33174E-	47239E-		90	306858E	.239531E-
$\frac{\pi}{\infty}$	16	29815	5934E		0.7	118478E	209380E-
18	17	53221E	<u>3</u>		08	16532E-	10169
18	18	18576E-	0.28969E-		60	14160E-	11673E-
				20	10	50519	0.249325E-7
10	00	360353E-			11	265501E	241596E-
10	01	831927E	4695		12	52711E	391129E-
<u>د</u> ا	05	134270E-	205615E-		13	23834E.	80699E-8
0	03	723332E-	6259		14	435379E	182584E
10	04	547610E-	44901E-		15	63460	43584E
13	05		12626E		16	12641E	69055E-
<u>c</u>	90	77506E-	0.474491E-7		17	16979E.	22005E-7
<u>c</u>	07	668100E	335062E		18	303597]	328549E
<u>c</u>	ς Σ	059483E	10055E-		19	27E-	-3666
<u>c</u>	0	232994E	15549E		20	.148501E	5208
10	10	143453E	30221E-				
c I	11	0.550503E-7	0.574992E-7	2.1	00	63622E	
-12	12	128344E	415871	2.1	01	22181E-7	306106E
<u>c</u>	13	228003E	0.31810E-10	21	05	25225E-	408729E-
<u>c</u>	14	30661E-	139066	2.1	03	424342E-	14107E-
<u>-</u>	15	_	•	21	04	0.101995E-7	-0.34651E-7
10	16	11124E-		21	90	406137E-	0.45851E-

"Real World" Normalized Geopotential Spherical Harmonic Coefficients (Continued) Table IV-3.

Snm	. 107119E	.51393E	.300204E	.18752E-	.29825E-	.67049E-	11	.19705E-		0	173212E-	338670E	203054E-	10493E-	20354区	312782E	201798E	13298E-	188708E	19015E-	2461	60050E-	54632E-	15876E-	236010E	12236E-	288960E	13375E-	120734E	28385	822857E		1061
$\overline{\mathtt{C}}_{\mathbf{n}\mathrm{m}}$	.493904E	.167609E-	.26816E-8	. 382741	.17776E-	.341486E	7985E-	.86883E		.42110E-	. 133217E	.179314E	.309501E	.256717E	.117139E	.398542E	.27806E-	.592375E	.99354E-	.305142E	19849	.463131E	.382767E	. 193972E	.21170E-	.129718E	200601E	.27388E-	.259457E	.27982E-	.148752E	-0.34170E-7	.51707E-
Σ	15						2.1			00	01	05	03	04	90	90	20	80	60	10	11	12	13	14	15	16	17	18	19	20	2.1	22	
Z	22																				23												
Snm	0.23154E	0.25265E-	0.38647E-	0.12631E-	0.10542E-	0.21976E-	.28885E-	0.13695E-	0.115217E-7	.197129E	0.42410E-	.44800E-	0.14446E-	.414327E	.356467	.20328E-		0	.23997E-	. 1280981		.250485E	0.17341E-	.32529E-	0.26561E-	. 31695	0.20429E-	0.53333E-	.20457E-	0.23631E-	.398652E	.658080E-	
Čnm	47136E-	21598	22307E-	227568E-	397897E-	696079E-	926007	383861E-		308850E	204000E-	608111E-	39750E-	303184E	17193E-	136428		26905E-	201011E	19709E-	-0.21604E-7	30189E-	32913E-	337159E-	384996E-	494668E	16983E-7	171803E	169672E-	24645E-	33008E-	49190E-	
M	90	0.7	80	60	10	11	12	13	14	15	16	17	18	<b>1</b> 0	20	2.1		00	0.1	05	03	04	90	90	07	80	00	10	11	12	13	14	
z	2.1	2.1	2.1	2 1	2.1	2.1	2.1		2.1												22												

Table IV-3. "Real World" Normalized Geopotential Spherical Harmonic Coefficients (Continued)

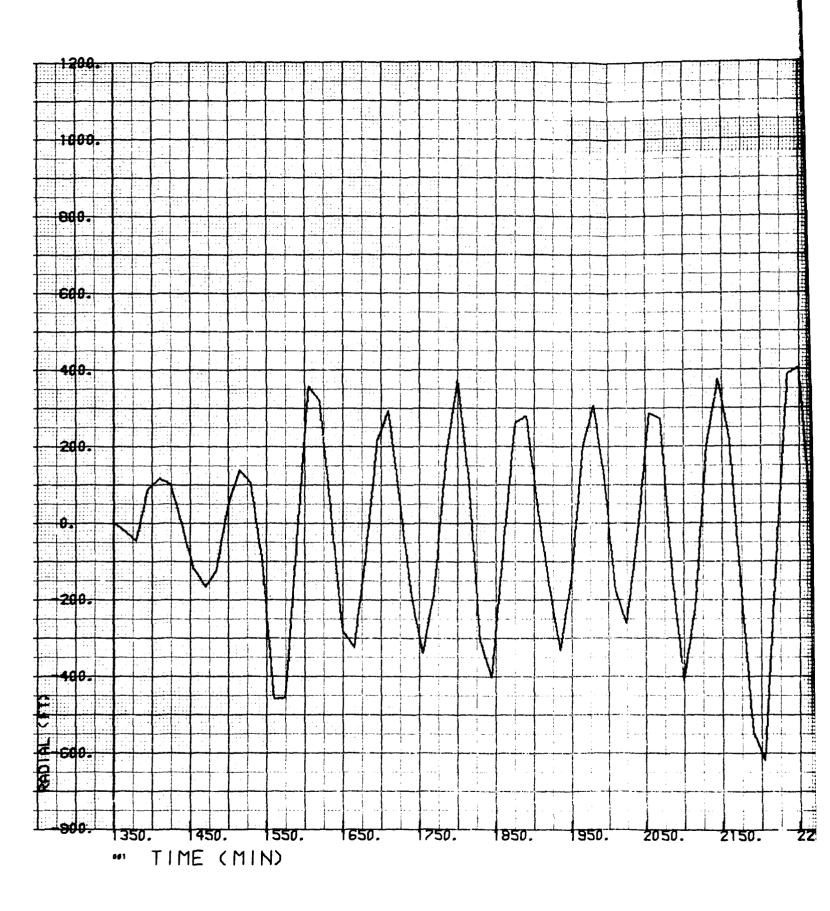
18         05         -0.32811E-8         0.799469E-7         19         17         0.373620E-7         -0.5486E-7         19         18         0.6         0.95303E-7         -0.4436E-7         19         18         0.89605EE-7         -0.54466E-7         19         18         0.89605EE-7         -0.54466E-7         19         18         0.0         0.19763E-7         -0.54466E-7         0.194618E-7         0.194618E-7         0.0         110         0.89465E-7         0.0         10.19763E-7         0.0         0.19763E-7         0.0         0.44465B-7         0.0         0.14763E-7         0.0         0.14763E-7         0.0         0.14763E-7         0.0         0.14774E-7         0.0         0.13878E-7         0.0         0.25792E-7         0.0         0.2473E-7         0.0         0.2473E-7         0.0         0.4426B-7         0.0         0.2473E-7         0.0         0.2473E-7         0.0         0.4474E-8         0.0         0.24746E-7         0.0         0.14474E-8         0.0         0.0         0.14474E-8         0.0         0.0         0.14474E-8         0.0         0.0         0.14474E-8         0.0         0.0         0.14474E-9         0.0         0.14474E-9         0.0         0.14474E-7         0.0         0.14474E-7         0.0	z	M	Çnnı	<del>S</del> nm	z	M	Ēnm	Snm
06         0.953033E-7         -0.34436E-7         19         18         0.890505E-7         -0.5456E-7         -0.5456E-7         -0.71969E-7         19         10         10         10         105453E-7         -0.5456E-7         -0.5456E-7         -0.1469E-7         0.014783E-7         -0.5456E-7         -0.5456E-7         0.014783E-7         0.014783E-7         0.014783E-7         0.014783E-7         0.014783E-7         0.014783E-7         0.014783E-7         0.014783E-7         0.014783E-7         0.0147847E-8         0.05467E-7         0.00306763E-7         0.02548         0.05407E-7         0.0306763E-7         0.04467E-7         0.05467E-7         0.04467E-7         0.04467E-7         0.04467E-7         0.04467E-7         0.04467E-7         0.04467E-7         0.04467E-7         0.04467E-7         0.04467E-7         0.044678E-7         0.044678E-8         0.044678E-7         0.044678E-7         0.044678E-8         0.044678E-8         0.044678E-8         0.044678E-8         0.044678E-8         0.044678E-8	18	90	-0.32811E-8	.799469E-	19	17	373620E-	58626E
07         -0.54556E_7         -0.71969E_7         19         19         -0.1753E_7         0.54256E_7           08         0.197630E_7         0.21351E_7         0.018785E_6         0         0.21351E_7         0.023351E_7         0.023351E_7         0.023351E_7         0.023351E_7         0.023351E_7         0.023351E_7         0.023351E_7         0.02453E_7         0.0244741E_7         0.02453E_7         0.02453E_7         0.02453E_7         0.02453E_7         0.02453E_7         0.02453E_7         0.02453E_7         0.02453E_7         0.02454E_7         0.02454E_7         0.02454E_7	18	90	0.953033E-7	.34436E-	19	18	890505E-	0.59496E-
08 0.197630E-7 0.194518E-7 0.0 0.108785E-6 0.23980E-7 0.65944E-7 0.213571E-7 20 0.3 3580E-7 0.23980E-1 10 0.48421E-8 0.56496E-7 20 0.3 3065163E-7 0.4042 0.236496E-7 20 0.3 3065163E-7 0.4042 0.236496E-7 20 0.3 3065163E-7 0.4042 0.236496E-7 20 0.3 3065163E-7 0.2495 0.236496E-7 0.65927E-7 20 0.3 306516E-8 0.2495 0.2495 0.231442E-7 0.65739E-7 20 0.5 306518E-7 0.298156E-7 0.47239E-7 20 0.5 306518E-7 0.298156E-7 0.125934E-7 20 0.5 306518E-7 0.298156E-7 0.18576E-7 0.28969E-7 20 0.9 0.22616E-8 0.2415 0.0 360353E-7 0.28969E-7 20 0.9 0.22616E-8 0.2415 0.0 360353E-7 0.269516E-7 20 0.9 0.22616E-8 0.2415 0.0 360353E-7 0.18576E-7 0.269516E-7 20 0.9 0.22616E-8 0.2415 0.0 360353E-7 0.18576E-7 0.269516E-7 20 0.0 360353E-7 0.1653E-7 0.1653E-7 0.1695E-6 20 0.256516E-8 0.2415 0.0 360353E-7 0.1653E-7 0.1695E-7 0.256516E-8 0.2415 0.0 36035E-7 0.1653E-7 0.1695E-6 20 0.149516E-7 0.241616E-7 0.241616E-7 0.256516E-8 0.256316E-8 0.256316E-7 0.136542E-7 0.141645E-7 0.256316E-7 0.14245E-7 0.24646E-7 0.256316E-7 0.25	18	07	-0.54536E-7	71969E-	19	19	17153E-	542653]
09         -0.65944E-7         0.21371E-7         20         0.108885E-6         0           10         -0.8783E-9         0.60542E-7         20         0.306683E-7         0.5136E-7         0.5298           11         0.249072E-8         -0.54946E-7         20         0.3365E-7         0.2145           12         0.254072E-8         -0.6597E-7         20         0.1332E-8         0.2145           13         0.230824E-7         -0.6711E-7         20         04         -0.25799E-7         0.2345           14         0.19840E-7         -0.6711E-7         20         04         -0.25799E-7         0.2345           16         0.298156E-7         -0.40716E-7         20         07         0.118478E-7         0.2346           17         -0.53221E-7         -0.40716E-7         20         07         0.118478E-7         0.2045           17         -0.53221E-7         -0.40716E-7         20         09         -0.25501E-8         0.2453           17         -0.53221E-7         -0.28969E-7         20         09         -0.25501E-8         0.2445           18         -0.18576E-7         -0.28969E-7         20         09         -0.25501E-7         -0.1016           1	18	80	0.197630E-7	194518E				
10         -0.87832E-9         0.605422E-7         20         01         -0.33580E-7         0.0298           11         0.498471E-8         -0.56496E-7         20         0.33580E-7         -0.4042           13         0.244671E-8         -0.56496E-7         0.03372E-8         0.2446           13         0.230824E-7         -0.67111E-7         20         04         -0.25799E-7         0.2446           14         0.198402E-7         -0.67111E-7         20         05         -0.7996E-8         0.2446           15         -0.33174E-7         -0.47239E-7         20         06         0.04958E-7         0.2093           16         0.298156E-7         -0.40204E-7         20         07         0.14878E-7         0.2093           17         -0.5322E-7         -0.40204E-7         20         09         -0.25160E-7         0.10167           18         -0.18576E-7         -0.28969E-7         20         09         -0.25160E-7         0.1673           18         -0.18576E-7         -0.28969E-7         20         09         -0.25160E-7         0.1673           18         -0.18576E-7         -0.28969E-7         20         09         -0.25160E-7         0.1673           <	18	60	-0.65944E-7	213571E		00	108785E-	0
11         0.498471E-8         -0.56496E-7         20         0.306763E-7         -0.404072E-8         -0.49071E-7         20         0.3322E-8         0.21452E-8         0.21462E-7         0.20942E-7         0.02941E-7         0.066         0.3068SBE-7         0.2994E-7         0.0696B-7	18	10	-0.87832E-9	605422E		01	0.33580E-	2298
12         0.264072E-8         -0.49071E-7         20         03         -0.1332E-8         0.2145           13         0.238824E-7         -0.6592E-7         20         04         -0.25799E-7         0.2961           14         0.138402E-7         -0.6592E-7         20         05         -0.25799E-7         0.2961           15         -0.33174E-7         -0.47239E-7         20         06         0.36685E-7         0.2394           16         0.298156E-7         -0.40016E-7         20         07         0.118478E-7         0.2093           17         -0.53221E-7         -0.40016E-7         20         08         -0.1653E-7         -0.1016           18         -0.18376E-7         -0.28969E-7         20         09         -0.250519E-8         0.2493           00         0.360353E-7         -0.28969E-7         20         10         0.250519E-7         -0.1167           01         0.8370E-7         -0.28969E-7         20         11         0.265501E-8         0.2493           02         0.134270E-7         -0.25051E-7         20         12         0.15241E-8         0.2493           03         0.72332E-8         -0.7656E-7         20         12         0.265501E-8<	18	11	498471E	0.56496E-		05	306763E	40429
13       0.230824E-7       -0.65927E-7       20       04       -0.25799E-7       0.2961         14       0.198402E-7       -0.67111E-7       20       05       -0.7996E-8       0.3343         15       -0.233174E-7       -0.67111E-7       20       06       0.36858E-7       0.2395         16       -0.298156E-7       -0.40016E-7       20       07       0.14678E-7       0.1016         17       -0.53221E-7       -0.40016E-7       20       08       -0.1653E-7       -0.1016         18       -0.18576E-7       -0.28969E-7       20       09       -0.29160E-7       -0.1167         00       0.360353E-7       -0.28969E-7       20       10       0.250519E-8       0.2493         01       0.381927E-8       0.146958E-6       20       11       0.265501E-8       0.2493         02       0.13332E-8       0.16579E-7       20       13       -0.25501E-8       0.2493         03       0.72332E-8       0.76579E-7       20       13       -0.265601E-8       0.1825         04       0.547610E-7       -0.12626E-6       20       15       -0.63460E-7       -0.13656E-7         05       -0.31882E-7       -0.12626E-6       20 <td>18</td> <td>12</td> <td>264072E</td> <td>0.49071E-</td> <td></td> <td>03</td> <td>0.13322E-</td> <td>214574E-</td>	18	12	264072E	0.49071E-		03	0.13322E-	214574E-
14         0. 198402E-7         -0.67111E-7         20         05         -0.7996E-8         0.343343           15         -0.33174E-7         -0.47239E-7         20         06         0.306858E-7         0.209395           16         0.298156E-7         -0.40016E-7         20         07         0.11847E-7         0.01016           17         -0.53221E-7         -0.28969E-7         20         09         -0.29160E-7         -0.1016           18         -0.18576E-7         -0.28969E-7         20         09         -0.29160E-7         -0.1167           18         -0.18576E-7         -0.28969E-7         20         09         -0.29160E-7         -0.1166           18         -0.18576E-7         -0.28969E-7         20         11         0.265501E-8         0.2493           01         0.360353E-7         0.26565E-6         20         12         0.255501E-8         0.2493           01         0.34270E-7         0.20551E-7         20         13         -0.23834E-8         -0.4358           02         0.134270E-7         -0.44901E-8         20         15         -0.63460E-7         -0.4358           05         -0.31882E-7         -0.12626E-6         20         15 <td< td=""><td>18</td><td>13</td><td>230824E</td><td>0.65927E-</td><td></td><td>04</td><td>0.25799E-</td><td>296186E</td></td<>	18	13	230824E	0.65927E-		04	0.25799E-	296186E
15       -0.33174E-7       -0.47239E-7       20       06       0.306858E-7       0.29395         16       0.298156E-7       -0.40016E-7       20       07       0.118478E-7       0.2093         17       -0.53221E-7       -0.40016E-7       20       08       -0.16532E-7       -0.1016         18       -0.18576E-7       -0.28969E-7       20       09       -0.29160E-7       -0.1167         00       0.360353E-7       -0.28969E-7       20       10       0.255501E-8       0.2493         01       0.831927E-8       0.146958E-6       20       12       0.255501E-8       0.2493         02       0.134270E-7       0.205615E-7       20       13       -0.255501E-8       0.2493         03       0.72333E-8       -0.76579E-7       20       13       -0.23834E-8       -0.8069         04       0.52332E-8       -0.76579E-7       20       14       0.435379E-7       -0.4358         05       -0.31882E-7       -0.44901E-8       20       15       -0.63460E-7       -0.4358         06       -0.7566E-7       -0.44901E-8       20       15       -0.63460E-7       -0.63560E-7         06       -0.31882E-7       -0.14646E-7 <t< td=""><td>18</td><td>14</td><td>198402E</td><td>0.67111E-</td><td></td><td>0.5</td><td>0.79996E-</td><td>334365E-</td></t<>	18	14	198402E	0.67111E-		0.5	0.79996E-	334365E-
16       0.298156E-7       0.125934E-7       20       07       0.118478E-7       0.2093         17       -0.53221E-7       -0.40016E-7       20       08       -0.16532E-7       -0.1016         18       -0.18576E-7       -0.28969E-7       20       09       -0.29160E-7       -0.1016         00       0.360353E-7       -0.28969E-7       20       10       0.255501E-8       0.2449         01       0.831927E-8       0.146958E-6       20       12       0.255501E-8       0.2453         02       0.134270E-7       0.205615E-7       20       13       -0.23834E-8       0.3918         03       0.72332E-8       -0.76579E-7       20       14       0.435379E-7       0.1825         04       0.547610E-7       -0.44901E-8       20       15       -0.63460E-7       -0.4358         05       -0.3182E-7       -0.44491E-7       20       15       -0.63461E-6       -0.63461E-6       -0.63461E-6       -0.033506E-7       -0.14641E-6       -0.03367E-7       -0.12641E-6       -0.033506E-7       -0.10655E-6       -0.014850E-7       -0.14850E-7       -0.14850E-7       -0.14850E-7       -0.14850E-7       -0.14850E-7       -0.14850E-7       -0.14850E-7       -0.14850E-7       -0.14850E	18	15	33174E-	0.47239E-		90	306858	239531E-
17       -0.53221E-7       -0.40016E-7       20       08       -0.16532E-7       -0.1016         18       -0.18576E-7       -0.28969E-7       20       09       -0.29160E-7       -0.1167         18       -0.18576E-7       -0.28969E-7       20       09       -0.29160E-7       -0.1167         00       0.360353E-7       0       146958E-6       20       11       0.265519E-8       0.2415         01       0.831927E-8       0.146958E-6       20       12       0.25551E-8       0.2493         02       0.134270E-7       0.265615E-7       20       13       -0.23334E-8       -0.24640E-7       0.33460E-7       0.33460E-7       0.435379E-7       0.4358         04       0.547610E-7       -0.44901E-8       20       15       -0.63460E-7       -0.4358         05       -0.31882E-7       -0.12626E-6       20       15       -0.63460E-7       -0.4358         06       -0.77506E-7       0.474491E-7       20       15       -0.16979E-7       -0.209         07       0.668100E-7       0.474491E-7       20       15       -0.16979E-7       -0.209         08       0.23294E-7       -0.10055E-6       20       15       -0.014850E-7	<b>1</b> 8	16	0.298156E-7	125934E		0.5	118478	209380E-
18       -0.18576E-7       -0.28969E-7       20       09       -0.29160E-7       -0.1167         00       0.360353E-7       0       0.250519E-8       0.2493         00       0.360353E-7       0       0.250519E-8       0.2493         01       0.831927E-8       0.146958E-6       20       12       0.152711E-7       0.3911         02       0.134270E-7       0.205615E-7       20       13       -0.2334E-8       -0.8069         03       0.72332E-8       -0.76579E-7       20       14       0.435379E-7       0.1825         04       0.547610E-7       -0.44901E-8       20       15       -0.63460E-7       -0.4358         05       -0.31882E-7       -0.44901E-8       20       15       -0.63460E-7       -0.4358         06       -0.77506E-7       -0.144491E-7       20       15       -0.63460E-7       -0.4358         07       0.6681000E-7       -0.15549E-7       20       15       -0.16579E-7       -0.2659         08       0.95948E-7       -0.15549E-7       -0.16549E-7       -0.16549E-7       -0.2059         09       0.23294E-7       -0.15549E-7       -0.20502E-7       -0.20502         11       0.50503E-7	18	17	-0.53221E-7	0.40016E-		80	0.165321	1016
00       0.360353E-7       0       0.250519E-8       0.2493         01       0.831927E-8       0.146958E-6       20       11       0.265501E-8       0.2415         01       0.831927E-8       0.146958E-6       20       12       0.152711E-7       0.3911         02       0.134270E-7       0.205615E-7       20       13       -0.23834E-8       -0.8069         03       0.72332E-8       -0.76579E-7       20       14       0.433379E-7       0.3911         04       0.547610E-7       -0.44901E-8       20       15       -0.6340E-7       0.14576E-7         05       -0.31882E-7       -0.44491E-7       20       15       -0.6340E-7       -0.4358         06       -0.77506E-7       0.474491E-7       20       17       -0.16979E-7       -0.2200         06       -0.77506E-7       0.335062E-7       20       17       -0.16979E-7       -0.209         06       -0.77506E-7       0.10055E-6       20       19       -0.10027E-7       -0.2509         09       0.22948E-7       -0.15549E-7       20       20       0.148501E-7       -0.2509         10       0.128344E-8       0.415871E-8       21       00       -0.522181E-7<	18	18	-0.18576E-7	0.28969E-		60	0.291601	11673E
00       0.360353E-7       0         01       0.831927E-8       0.146958E-6       20       12       0.152711E-7       0.3911         02       0.134270E-7       0.205615E-7       20       13       -0.23834E-8       -0.8069         03       0.72333E-8       -0.76579E-7       20       14       0.435379E-7       0.3911         04       0.547610E-7       -0.44901E-8       20       15       -0.63460E-7       -0.43539E-7         05       -0.31882E-7       -0.12626E-6       20       16       -0.63460E-7       -0.43539E-7         06       -0.31882E-7       -0.12626E-6       20       15       -0.63460E-7       -0.43539E-7         06       -0.31882E-7       -0.12626E-6       20       16       -0.16979E-7       -0.6905         06       -0.77506E-7       0.474491E-7       20       17       -0.16979E-7       -0.2200         07       0.668100E-7       -0.10055E-6       20       17       -0.16979E-7       -0.2099         08       0.523994E-7       -0.33221E-7       -0.33221E-7       -0.33221E-7       -0.232994E-7       -0.332321E-7         10       0.12834E-8       0.415871E-8       21       0.0222255E-7       0.4083						10	250519E	249325E-
01       0.831927E-8       0.146958E-6       20       12       0.152711E-7       0.3911         02       0.134270E-7       0.205615E-7       20       13       -0.23834E-8       -0.8069         03       0.72333E-8       -0.76579E-7       20       14       0.435379E-7       0.1825         04       0.547610E-7       -0.44901E-8       20       15       -0.63460E-7       -0.4358         05       -0.31882E-7       -0.12626E-6       20       16       -0.12641E-6       -0.6905         06       -0.77506E-7       0.474491E-7       20       17       -0.16979E-7       -0.6905         07       0.668100E-7       0.474491E-7       20       17       -0.16979E-7       -0.2200         08       0.959483E-7       -0.10055E-6       20       19       -0.16979E-7       -0.2099         09       0.232994E-7       -0.105549E-7       20       20       0.148501E-7       -0.2099         09       0.232994E-7       -0.30221E-7       20       20       0.148501E-7       -0.2099         10       0.143453E-7       -0.30221E-7       20       20       0.148501E-7       0.305218E-7         12       0.128344E-8       0.31810E-10	19	00	360353E	0		11	265501E	241596E
02       0.134270E-7       0.205615E-7       20       13       -0.23834E-8       -0.80699         03       0.72333E-8       -0.76579E-7       20       14       0.435379E-7       0.18258         04       0.547610E-7       -0.44901E-8       20       15       -0.63460E-7       -0.43584         05       -0.31882E-7       -0.12626E-6       20       16       -0.12641E-6       -0.69055         06       -0.77506E-7       0.474491E-7       20       17       -0.16979E-7       -0.69055         07       0.668100E-7       0.335062E-7       20       17       -0.16979E-7       -0.22009         08       0.959483E-7       -0.10055E-6       20       19       -0.16979E-7       -0.2099         09       0.232994E-7       -0.15549E-7       20       20       0.148501E-7       -0.2099         10       0.143453E-7       -0.30221E-7       21       00       -0.63622E-7       -0.2099         11       0.550503E-7       -0.31810E-10       21       0.0       -0.63622E-7       0.30610         12       0.128344E-8       0.415871E-8       21       00       -0.622255E-7       0.40872         14       -0.30661E-7       -0.76155E-7	10	01	831927E	146958E-		12	152711E	391129圧-
03 0.72332E-8 -0.76579E-7 20 14 0.435379E-7 0.18258 04 0.547610E-7 -0.44901E-8 20 15 -0.63460E-7 -0.43584 05 -0.31882E-7 -0.12626E-6 20 16 -0.12641E-6 -0.69055 06 -0.77506E-7 0.474491E-7 20 17 -0.16979E-7 -0.22009 07 0.668100E-7 0.335062E-7 20 17 -0.16979E-7 -0.22009 08 0 959483E-7 -0.10055E-6 20 19 -0.10027E-7 0.32854 09 0.232994E-7 -0.15549E-7 20 20 0.148501E-7 0.25999 11 0.550503E-7 0.3021E-7 21 00 -0.63622E-7 0.30616 12 0.128344E-8 0.415871E-8 21 01 -0.22181E-7 0.40872 13 0.228003E-7 0.31810E-10 21 02 0.25255E-7 0.40872 14 -0.30661E-7 0.1454E-7 21 05 0.401995E-7 -0.34651 16 -0.11124E-6 -0.14544E-7 21 05 0.406187E-7 -0.45851	19	05	134270E	205615E-		13	0.23834E-	0.8069
04       0.547610E-7       -0.44901E-8       20       15       -0.63460E-7       -0.43584         05       -0.31882E-7       -0.12626E-6       20       16       -0.12641E-6       -0.69055         06       -0.77506E-7       0.474491E-7       20       17       -0.16979E-7       -0.69055         07       0.668100E-7       0.335062E-7       20       17       -0.16979E-7       -0.22005         08       0.959483E-7       -0.10055E-6       20       19       -0.10027E-7       -0.20999         09       0.232994E-7       -0.3624E-7       20       20       19       -0.10027E-7       -0.20999         10       0.143453E-7       -0.30221E-7       20       20       0.148501E-7       0.2552         11       0.556503E-7       -0.3674992E-7       21       00       -0.63622E-7       0.2552         12       0.128344E-8       0.415871E-8       21       00       -0.63622E-7       0.40872         13       0.228003E-7       0.31810E-10       21       02       252255E-7       0.40872         14       -0.3661E-7       -0.76155E-7       21       03       0.424342E-7       -0.14107         15       -0.11124E-6       -0	19	03	723332E	0.76579E-		14	435379E	182584E
05       -0.31882E-7       -0.12626E-6       20       16       -0.12641E-6       -0.69059         06       -0.77506E-7       0.474491E-7       20       17       -0.16979E-7       -0.22009         07       0.668100E-7       0.335062E-7       20       17       -0.16979E-7       -0.22009         08       0.959483E-7       -0.10055E-6       20       19       -0.10027E-7       -0.20999         09       0.232994E-7       -0.15549E-7       20       20       0.148501E-7       -0.20999         10       0.143453E-7       -0.30221E-7       20       20       0.148501E-7       0.2552         11       0.550503E-7       -0.30221E-7       21       00       -0.63622E-7       0.2552         12       0.128344E-8       0.415871E-8       21       01       -0.22181E-7       0.30616         13       0.228003E-7       0.31810E-10       21       02       252255E-7       0.40872         14       -0.30661E-7       -0.76155E-7       21       03       0.424342E-7       -0.14107         15       -0.118375E-7       -0.14544E-7       21       05       0.406187E-7       -0.34651	61	04	547610E	0.44901E-		15	0.63460E-	0.43584E-
06       -0.77506E-7       0.474491E-7       20       17       -0.16979E-7       -0.22005         07       0.668100E-7       0.335062E-7       20       15       0.303597E-7       0.32854         08       0.959483E-7       -0.10055E-6       20       19       -0.10027E-7       -0.20999         09       0.232994E-7       -0.30221E-7       20       20       0.148501E-7       -0.25520         10       0.143453E-7       -0.30221E-7       21       00       -0.63622E-7       0.25520         11       0.550503E-7       0.574992E-7       21       00       -0.63622E-7       0.30610         12       0.128344E-8       0.415871E-8       21       01       -0.22181E-7       0.30610         13       0.228003E-7       0.31810E-10       21       02       0.25255E-7       0.40872         14       -0.30661E-7       -0.76155E-7       21       04       0.101995E-7       -0.14107         15       -0.11124E-6       -0.14544E-7       21       05       0.406187E-7       -0.34651	19	05	31882E-	0.12626E-		16	0.12641E-	0.69055
07       0.668100E-7       0.335062E-7       20       1f       0.303597E-7       0.32854         08       0.959483E-7       -0.10055E-6       20       19       -0.10027E-7       -0.209999         09       0.232994E-7       -0.15549E-7       20       20       0.148501E-7       -0.20999         10       0.143453E-7       -0.30221E-7       21       00       -0.6362E-7       0.25520         11       0.550503E-7       0.574992E-7       21       00       -0.6362E-7       0.30610         12       0.128344E-8       0.415871E-8       21       01       -0.22181E-7       0.30610         13       0.228003E-7       0.31810E-10       21       02       0.252255E-7       0.40872         14       -0.30661E-7       -0.76155E-7       21       04       0.101995E-7       -0.14107         15       -0.11124E-6       -0.14544E-7       21       05       0.406187E-7       -0.45851	61	90	77506E-	474491E		17	0.16979圧-	0.22005E-
08 0 959483E-7 -0.10055E-6 20 19 -0.10027E-7 -0.209999 0.232994E-7 -0.15549E-7 20 20 0.148501E-7 0.25520 10 0.143453E-7 -0.30221E-7 21 00 -0.63622E-7 0.550503E-7 0.415871E-8 21 01 -0.22181E-7 0.30610 14 -0.30661E-7 0.139066E-7 21 03 0.424342E-7 0.14107 15 -0.18375E-7 -0.76155E-7 21 05 0.406187E-7 -0.34651 16 -0.11124E-6 -0.14544E-7 21 05 0.406187E-7 -0.45851	19	07	668100E-	335062E		1 ک	303597E	. 32854
09 0.232994E-7 -0.15549E-7 20 20 0.148501E-7 0.25520 10 0.143453E-7 -0.30221E-7 11 0.550503E-7 0.574992E-7 21 00 -0.63622E-7 0 12 0.128344E-8 0.415871E-8 21 01 -0.22181E-7 0.30610 13 0.228003E-7 0.31810E-10 21 02 0.25255E-7 0.40872 14 -0.30661E-7 0.139066E-7 21 03 0.424342E-7 -0.14107 15 -0.18375E-7 -0.76155E-7 21 05 0.406187E-7 -0.34651 16 -0.11124E-6 -0.14544E-7 21 05 0.406187E-7 -0.45851	19	80	959483E-	0.10055E-		19	0.10027E-	0.20999E-
10 0.143453E-7 -0.30221E-7	19	60	232994E-	0.15549E-			148501]	.255208]
11     0.550503E-7     0.574992E-7     21     00     -0.6362E-7     0       12     0.128344E-8     0.415871E-8     21     01     -0.22181E-7     0.30610       13     0.228003E-7     0.31810E-10     21     02     0.552255E-7     0.40872       14     -0.30661E-7     0.139066E-7     21     03     0.424342E-7     -0.14107       15     -0.18375E-7     -0.76155E-7     21     05     0.101995E-7     -0.34651       16     -0.11124E-6     -0.14544E-7     21     05     0.406187E-7     -0.45851	10	10	143453E-	.30221E-				
12 0.128344E-8 0.415871E-8 21 01 -0.22181E-7 0.30610 13 0.228003E-7 0.31810E-10 21 02 0.252255E-7 0.40872 14 -0.30661E-7 0.139066E-7 21 03 0.424342E-7 -0.14107 15 -0.18375E-7 -0.76155E-7 21 04 0.101995E-7 -0.34651 16 -0.11124E-6 -0.14544E-7 21 05 0.406187E-7 -0.45851	19	11	550503E-	.574992E	-	00	63622E-	0
13     0.228003E-7     0.31810E-10     21     02     0.252255E-7     0.40872       14     -0.30661E-7     0.139066E-7     21     03     0.424342E-7     -0.14107       15     -0.18375E-7     -0.76155E-7     21     04     0.101995E-7     -0.34651       16     -0.11124E-6     -0.14544E-7     21     05     0.406187E-7     -0.45851	19	12	128344E-	.415871E-		01	0.22181E-	306106
14 -0.30661E-7 0.139066E-7 21 03 0.424342E-7 -0.14107 15 -0.18375E-7 -0.76155E-7 21 04 0.101995E-7 -0.34651 16 -0.11124E-6 -0.14544E-7 21 05 0.406187E-7 -0.45851	<b>1</b> 0	13	228003E-	.31810E-1	-	70	25225E	408729E-
15 -0.18375E-7 -0.76155E-7 21 04 0.101995E-7 -0.34651 16 -0.11124E-6 -0.14544E-7 21 05 0.406187E-7 -0.45851	10	14	30661E-	.139066E-		03	424342E	0.14107E-
16 -0.11124E-6 -0.14544E-7   21 05 0.406187E-7 -0.45851	<b>0 I</b>	15	18375E-	0.76155E-		04	101995E	0.34651
	10	16	11124E-	0.14544E		90	406187E	.45851E-

Table IV-3. "Real World" Normalized Geopotential Spherical Harmonic Coefficients (Continued)

z	×	$\bar{C}_{ m nm}$	Snm	Z	M	$\bar{c}_{ m nm}$	$\overline{S}_{\mathrm{nm}}$
24	00	0.422303E-7	0	24	13	0.249900E-7	-0.20730E-8
24	01	-0.15215E-8	-8 -0.34873E-7	24	14	-0.53486E-7	-0.12466E-8
24	05	0.108446E-7	0.151859E-7	24	15	0.535485E-7	-0.82034E-8
24	03	0.211630E-7	0.207832E-8	24	16		-0.10137E-7
24	04	-0.31688E-7	-0.61802E-8	24	17	-0.11024E-7	
24	90	0.101969E-7	-0.11732E-7	24	18		
24	90	0.203522E-7	0.121721E-8	24	19	0.107197E-7	-0.33855E-7
24	07	0.339597E-7	-0.32352E-7	24	20	291973E	-0.22154E-7
24	08	0.251321E-7	-0.32292E-7	24	2.1	-0.17687E-7	-0.16306E-7
24	60	-0.88687E-8	0.281510E-7	24	22	0.158528E-7	
24	10	-0.27586E-7	0.406940E-8	24	23	0.303773E-7	15012E.
24	11	0.100996E-7	-0.18150E-7	24	24	0.270652E-7	-0.33997E-7
24	12	-0.43977E-8	-0.12029E-7				

Next a difference run was made between the reference model and the model defined by Table IV-3, the simulated gravity field. These in-track, radial, and cross-track differences are presented in Figures IV-2a, b, and c. The in-track difference shows a secular growth of approximately 280 ft/rev plus two periodic components: one with a period of 1 rev and an amplitude of approximately 800 ft and the other with a period of about 12 revs and an amplitude of 1300 ft. The radial difference plot shows a 1 rev periodic component with maximum amplitude of approximately 700 ft, as does the cross-track difference plot. As before, these data do not include an atmosphere force model.

It was concluded from these results that the simulated gravity field produces orbit perturbations which differ significantly from those of the nominal gravity field but which are not unrealistically large. The results of these difference runs should not be interpreted as estimates of ephemeris uncertainties, since by suitable orbit determination techniques these differences would be drastically reduced in actual practice. The plots illustrate one of the possible shortcomings of this simulated model, i.e., the field is too smooth. Although this field is as extensive as the present state of the art, there is reason to believe that a 24th degree and order model is still significantly smoother than that experienced by a vehicle moving in the earth's gravity field.



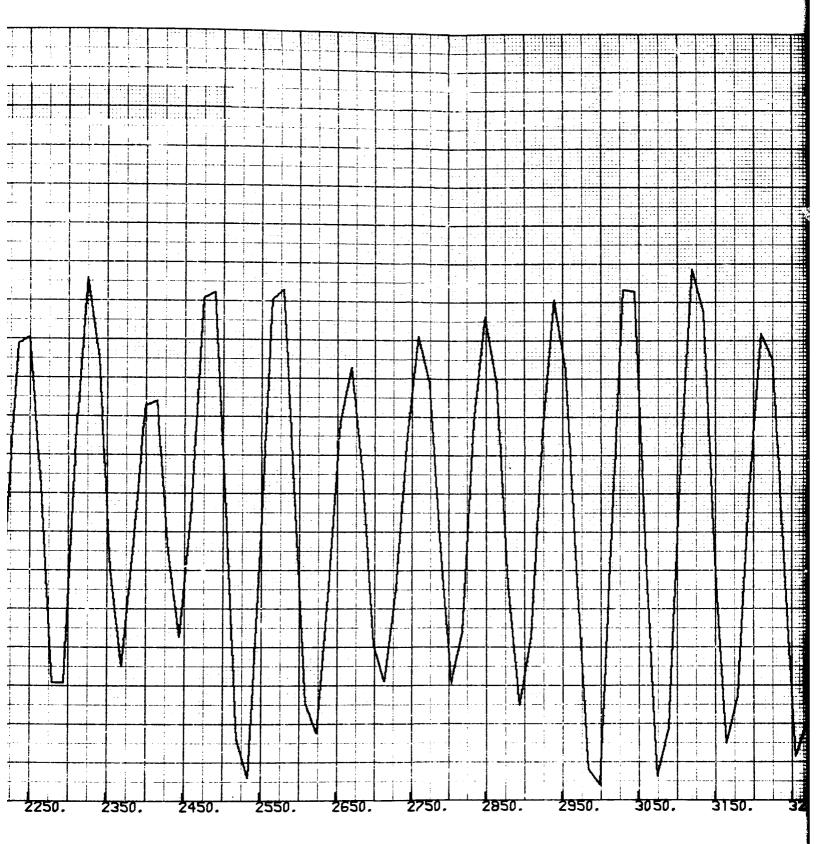


Figure IV-ia. Intrack Difference Between "Model" (
and Reference Geopotential (19, 19) A

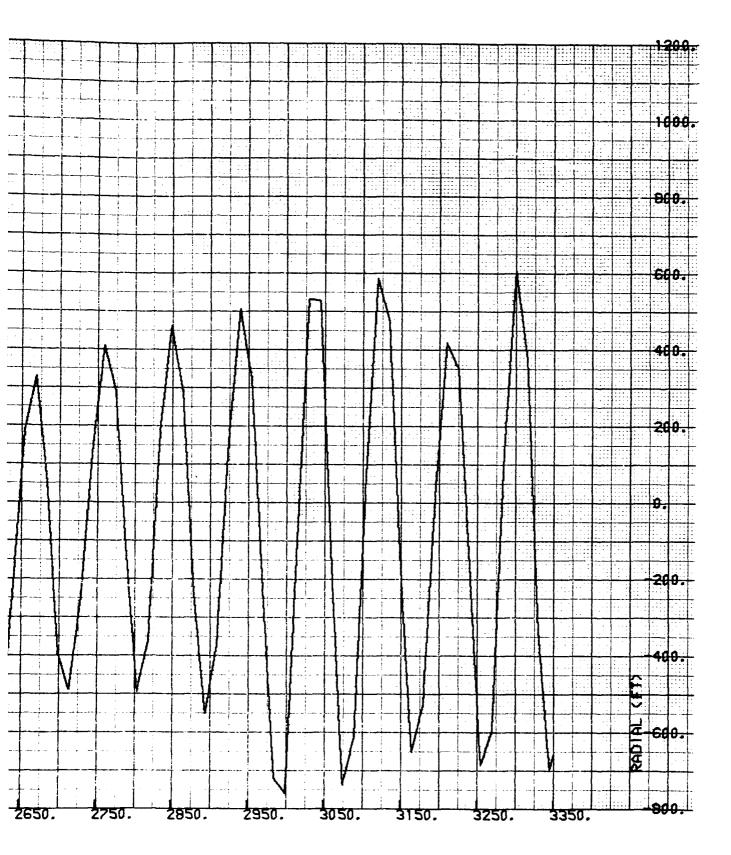
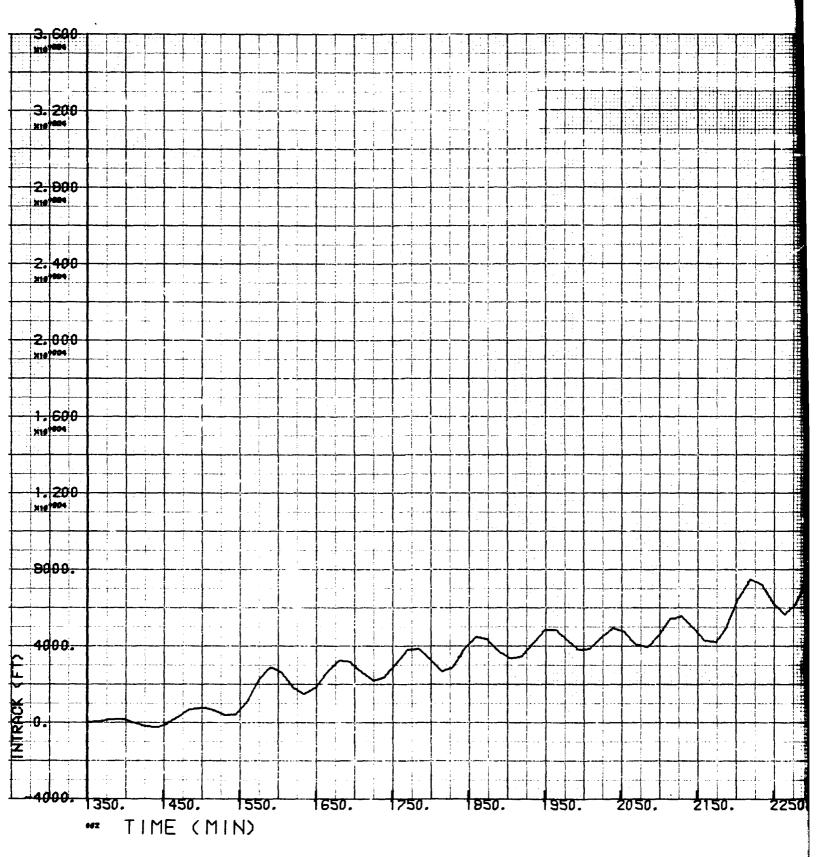


Figure IV-ia. Intrack Difference Between "Model" (6, 6) Geopotential and Reference Geopotential (19, 19) Atmosphere



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A

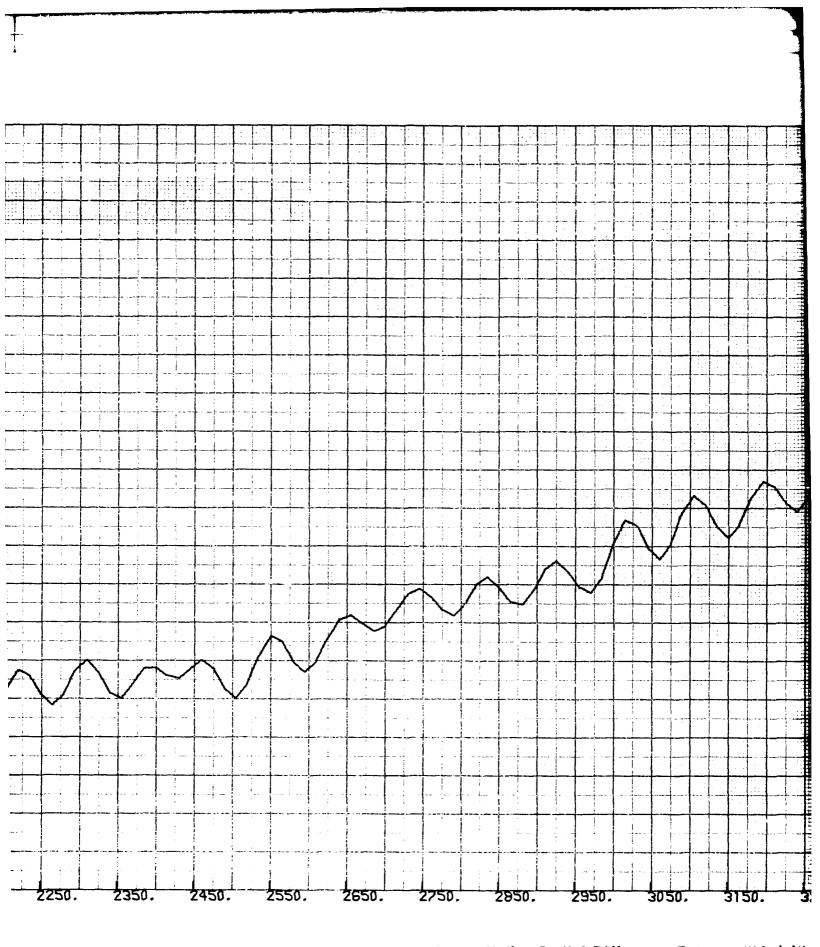


Figure IV-ib. Radial Difference Between "Model"

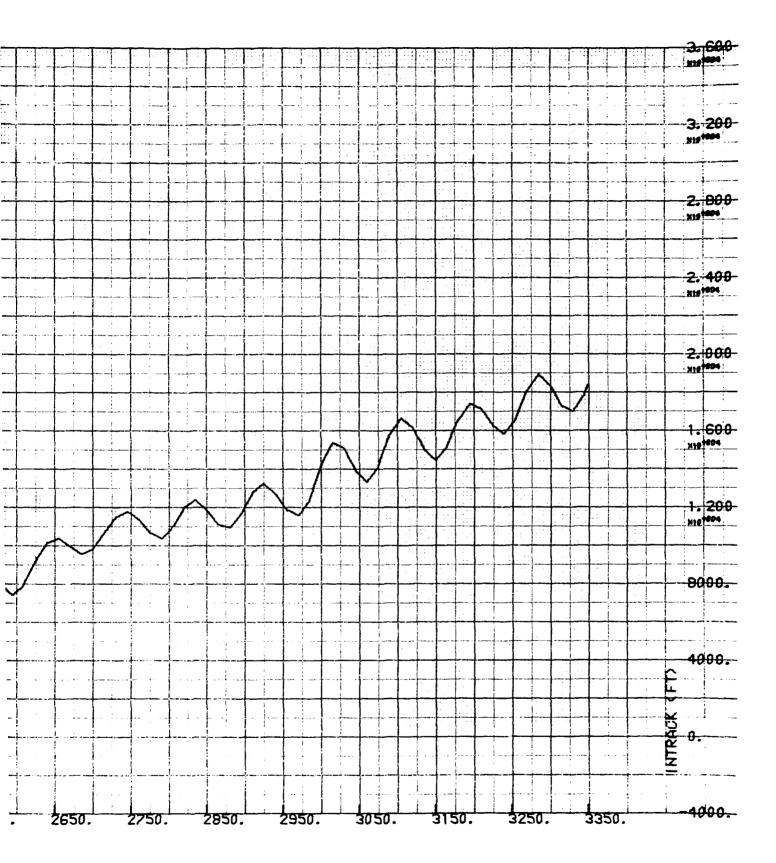
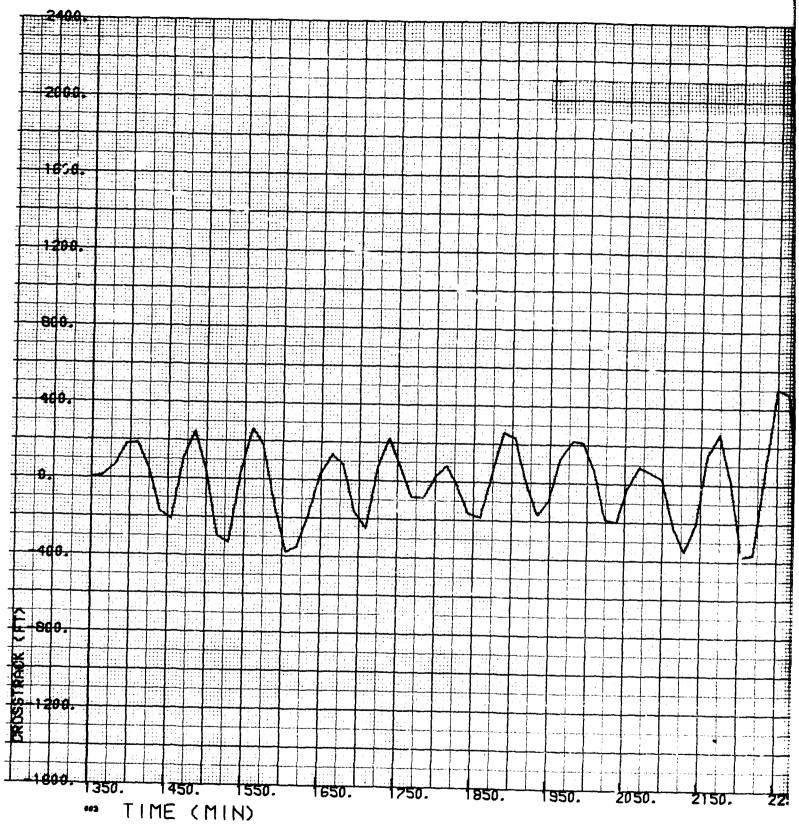


Figure IV-ib. Radial Difference Between "Model" and Reference



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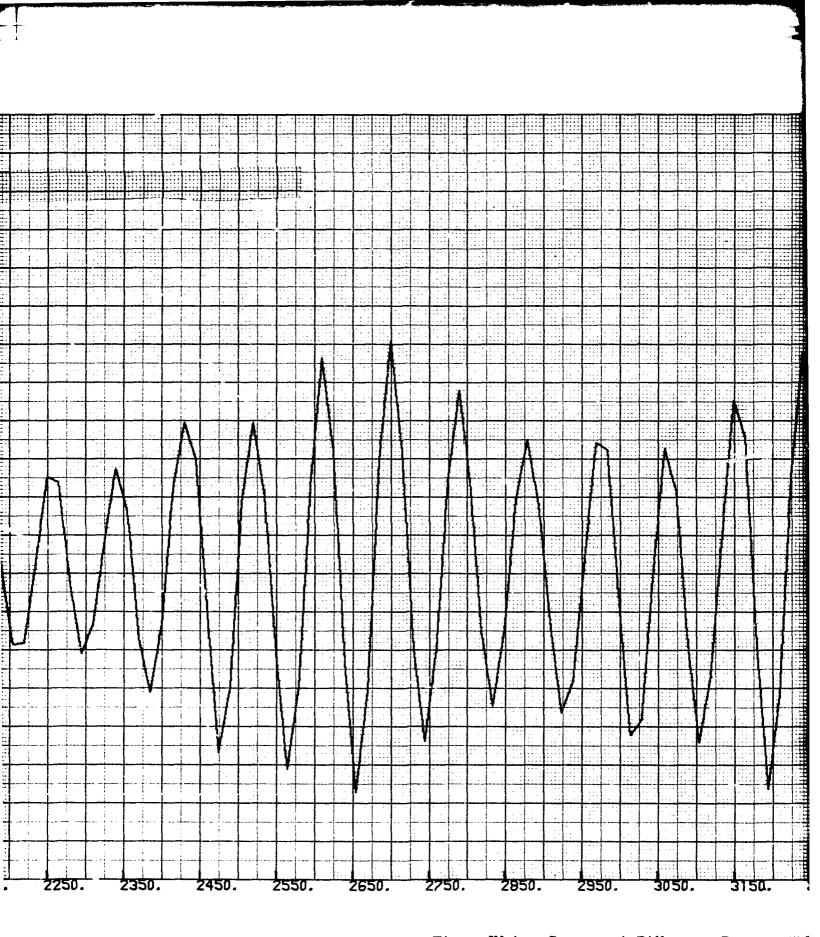


Figure IV-ic. Crosstrack Difference Between "M

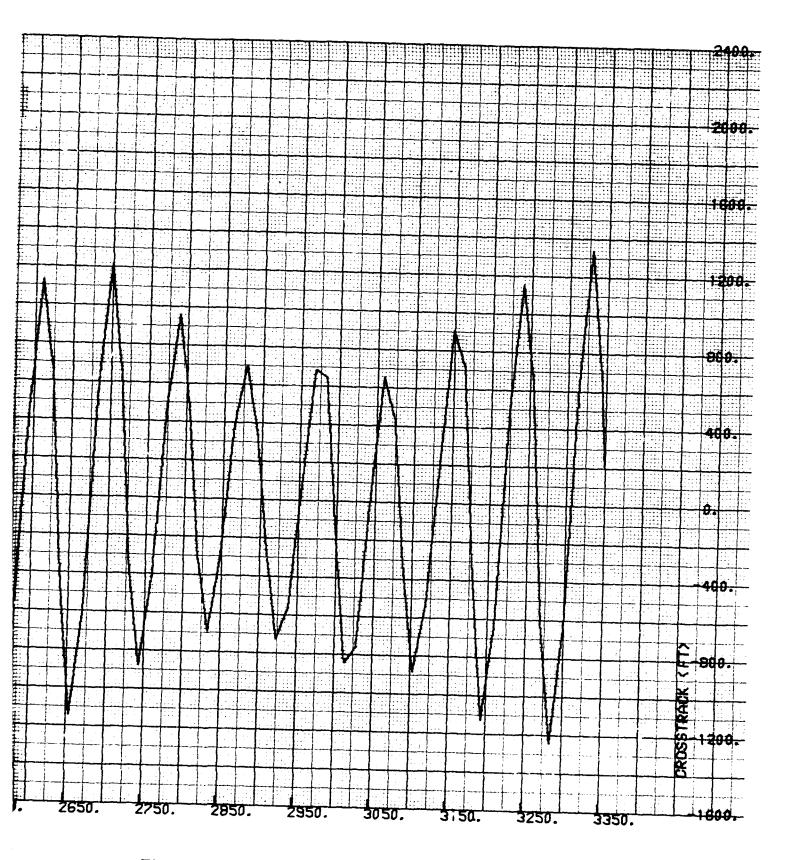
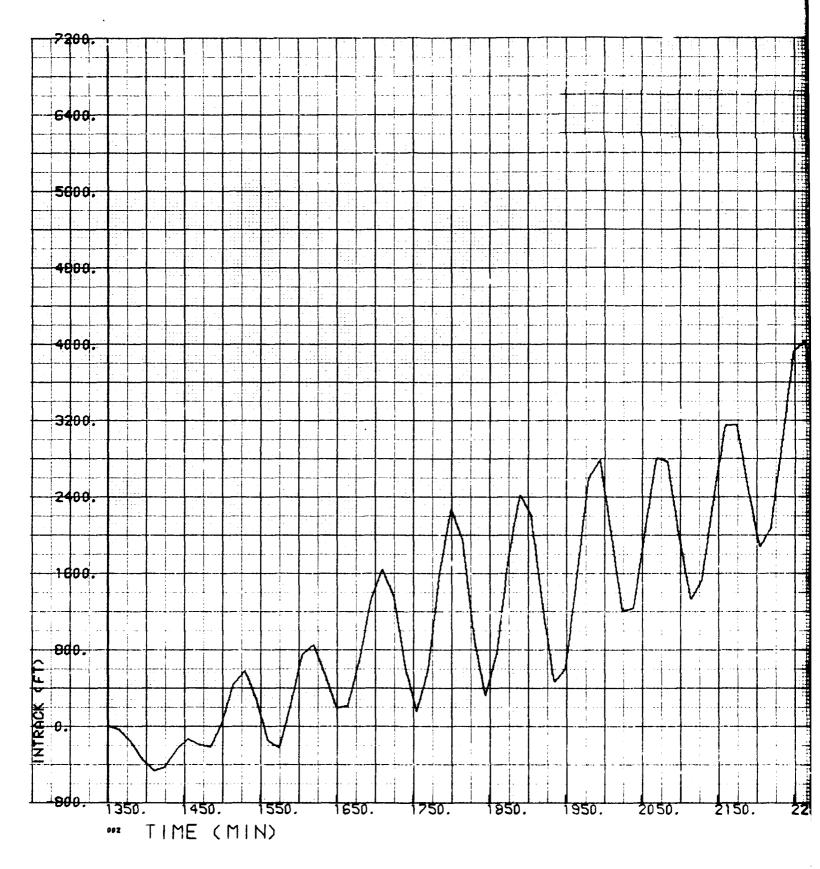


Figure IV-ic. Crosstrack Difference Between "Model" and Reference



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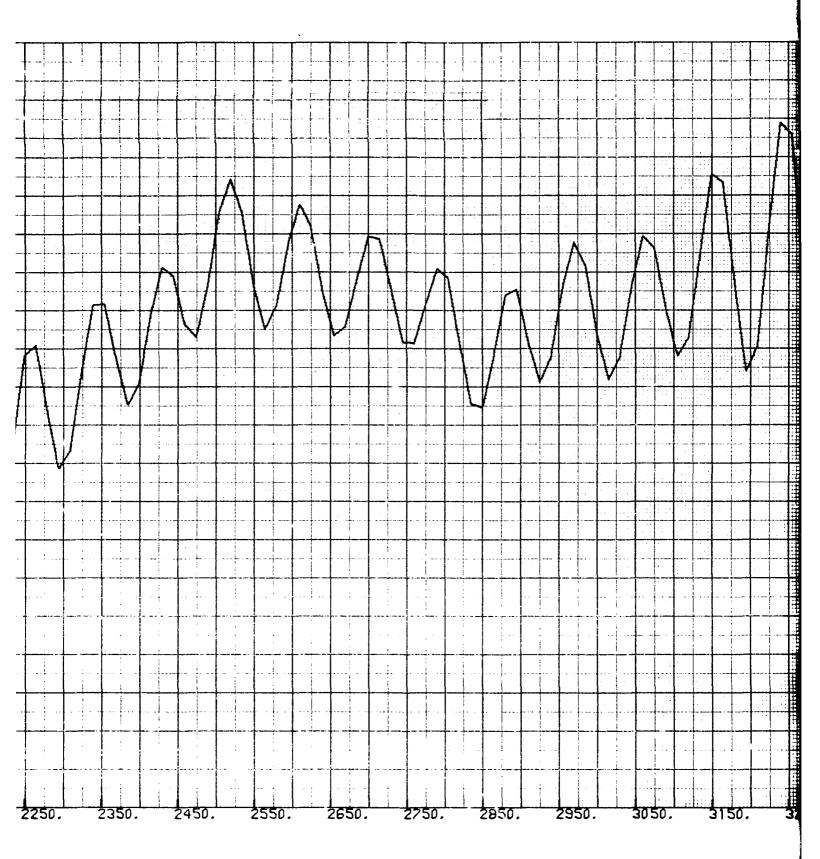


Figure IV-2a. Intrack Difference Getween Reference "Real World" Geopotentials

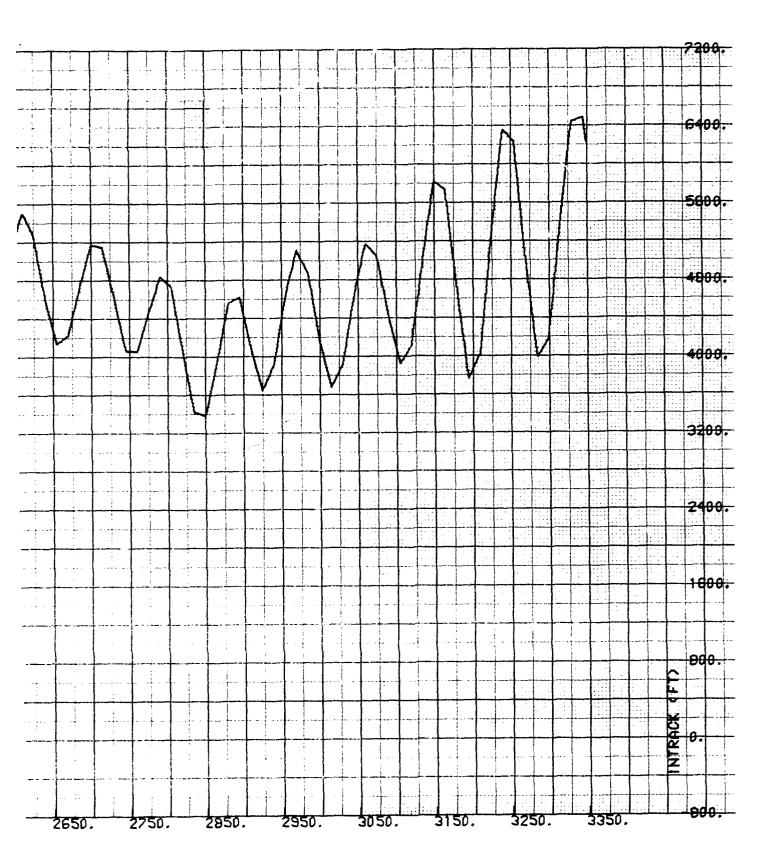
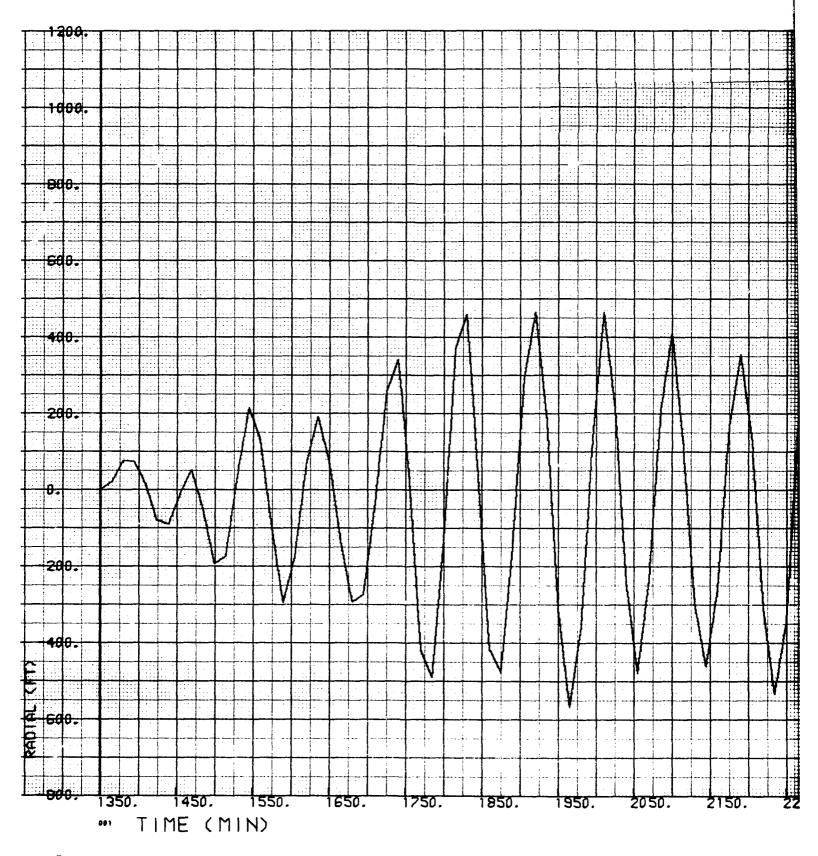


Figure IV-2a. Intrack Difference Getween Reference and "Real World" Geopotentials



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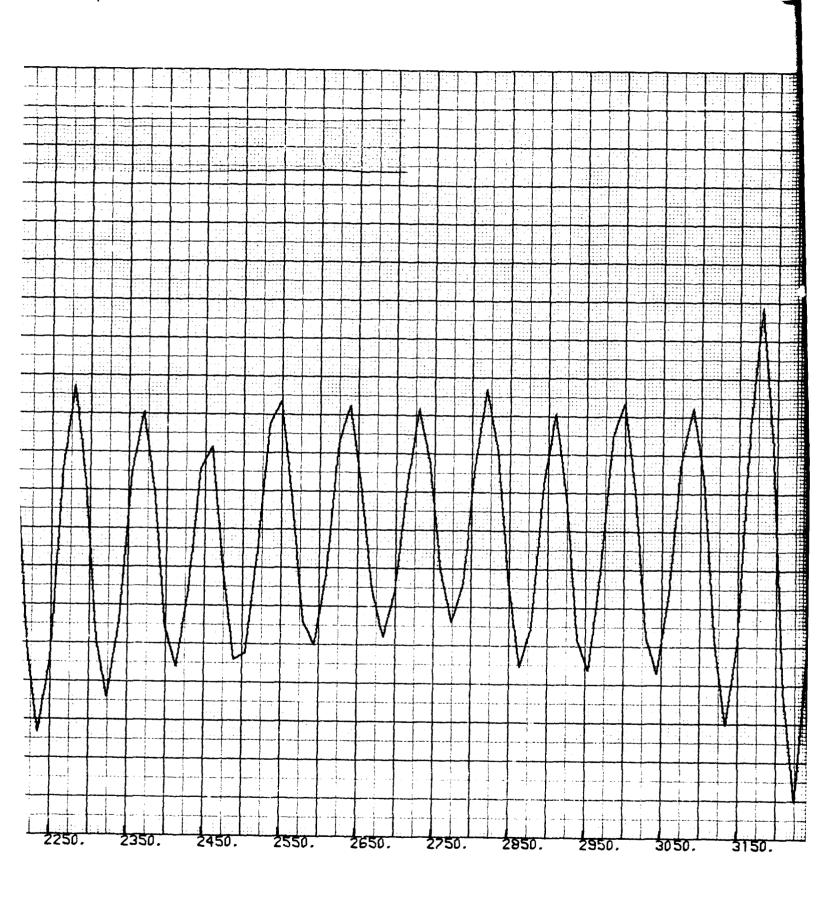


Figure IV-2b. Radial Difference Between Refer and "Real World" Geopotentials

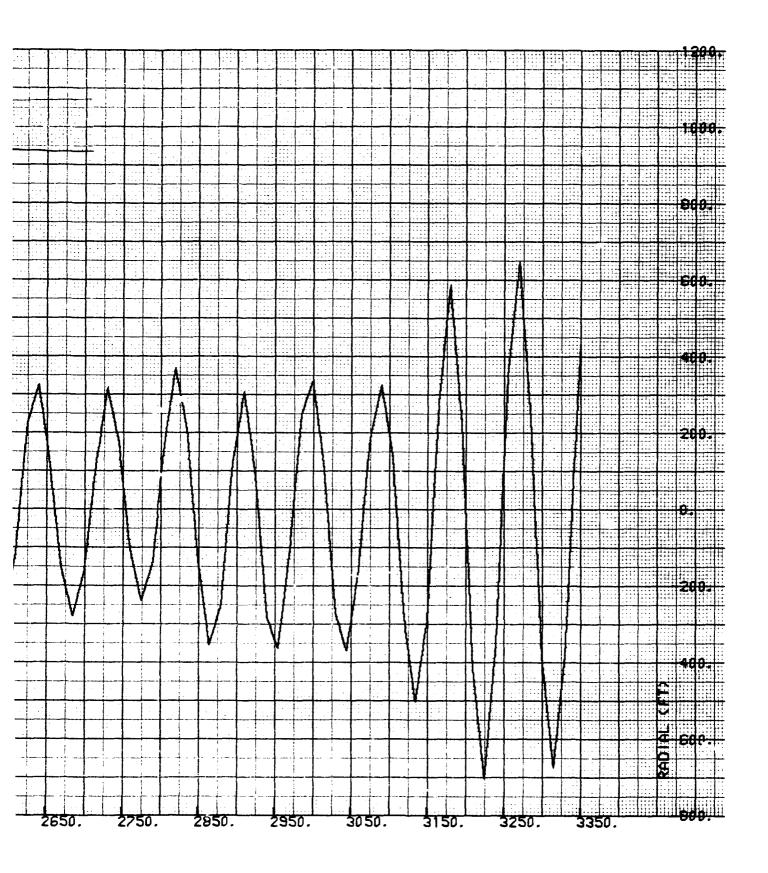
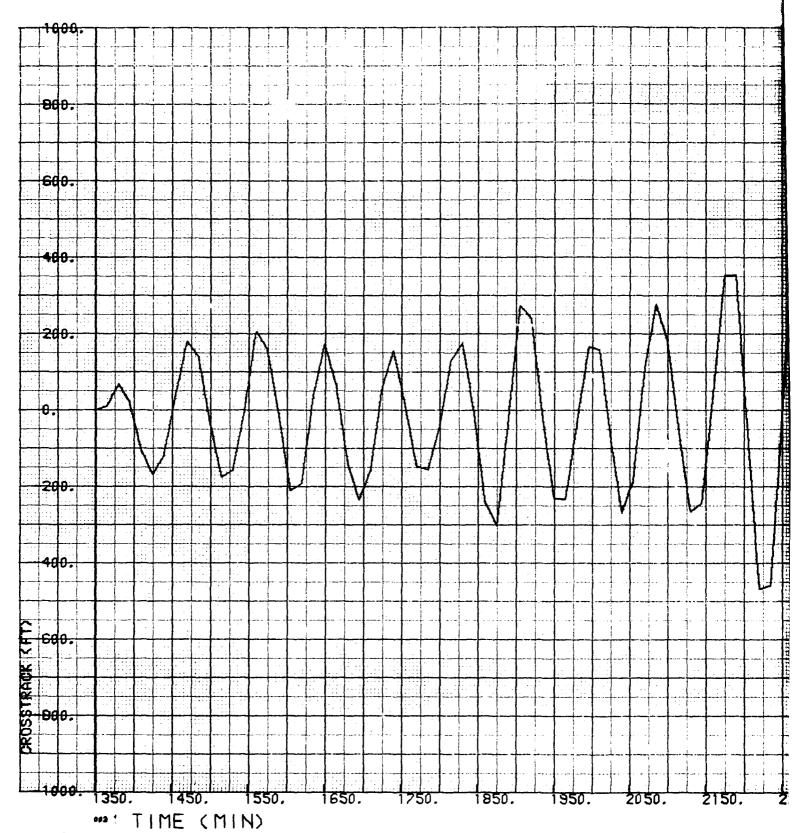


Figure IV-2b. Radial Difference Between Reference and "Real World" Geopotentials



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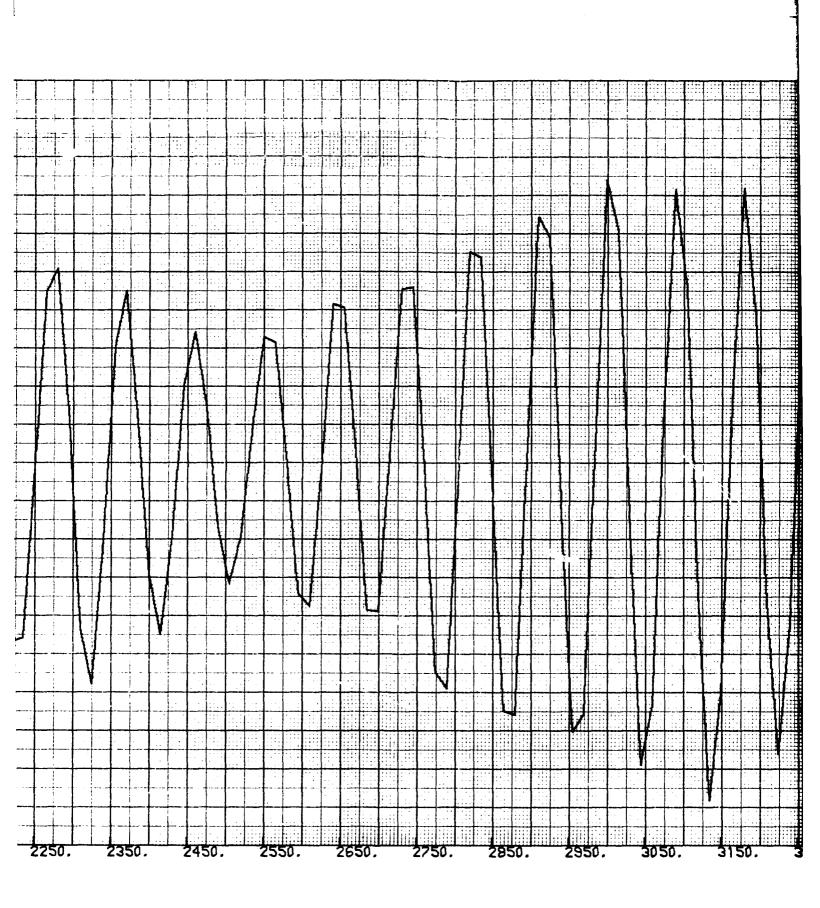


Figure IV-2c. Crosstrack Difference Between Reand "Real World" Geopotentials

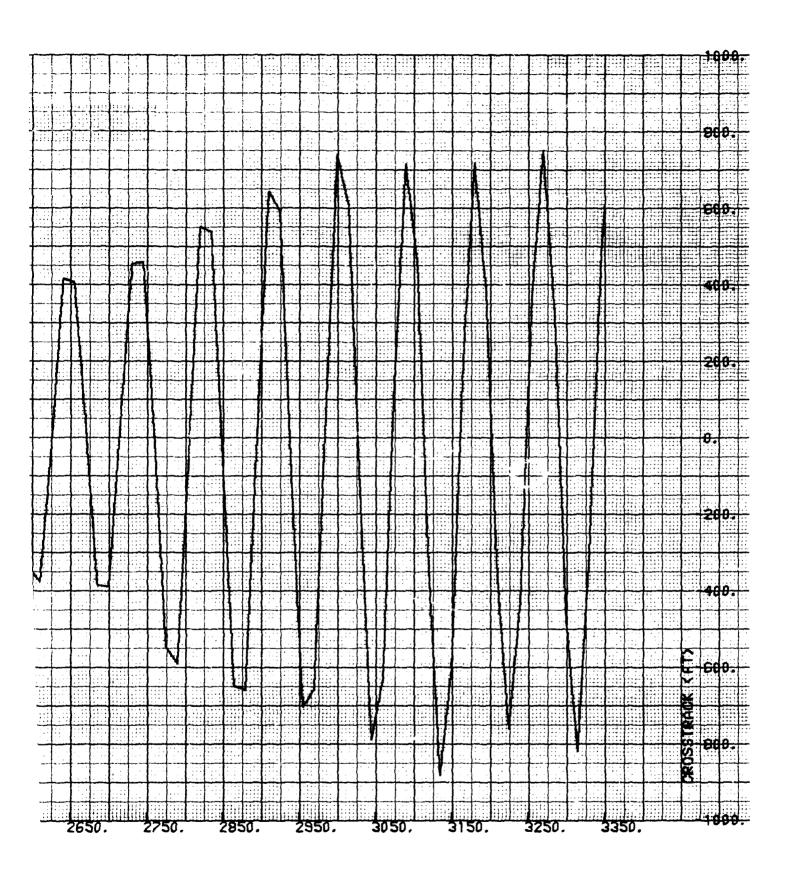


Figure IV-2c. Crosstrack Difference Between Reference and "Real World" Geopotentials

#### SECTION V

#### "REAL WORLD" DRAG MODEL

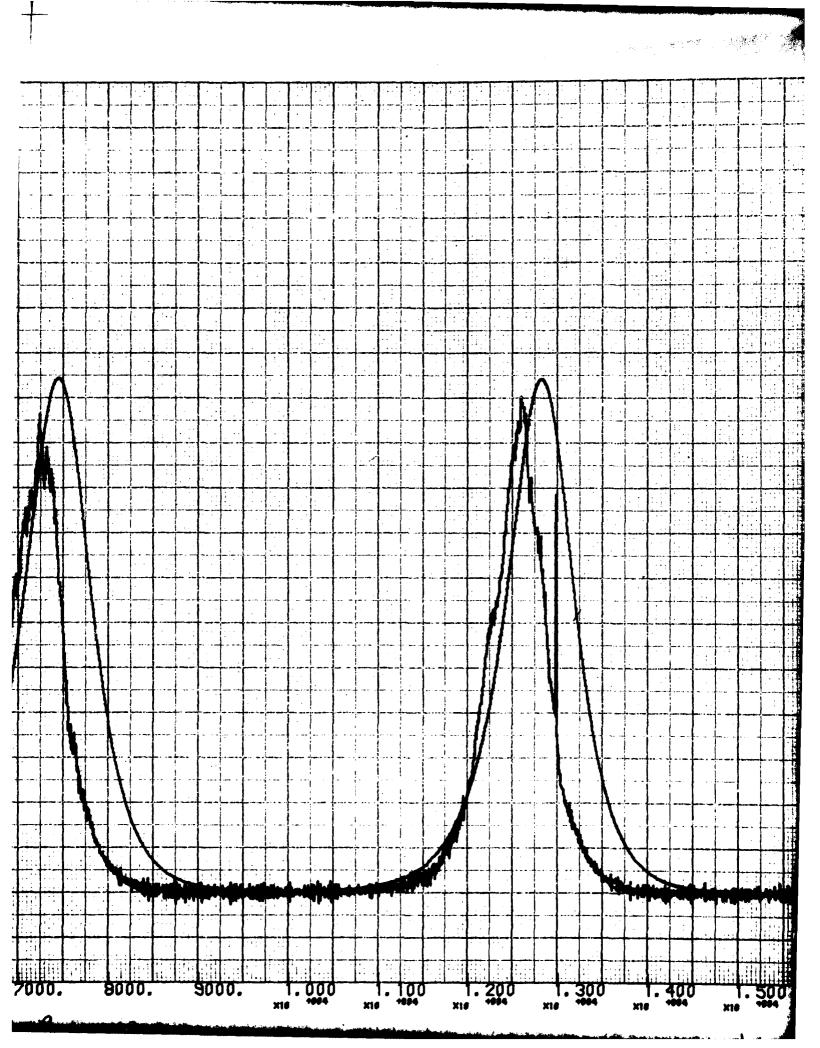
To obtain real world atmosphere data, the acceleration profile experienced by the first in a recent series of low altitude satellites to have an on-board low-g accelerometer was utilized. The orbital elements of this density measurement system (DMS) vehicle were quite close to those of the reference orbit. This suggested that the accelerometer data from the DMS - suitably scaled - could be used as an input real world drag profile to the ANS reference vehicle. Approximately 20 revs of continuous DMS data were available for this purpose.

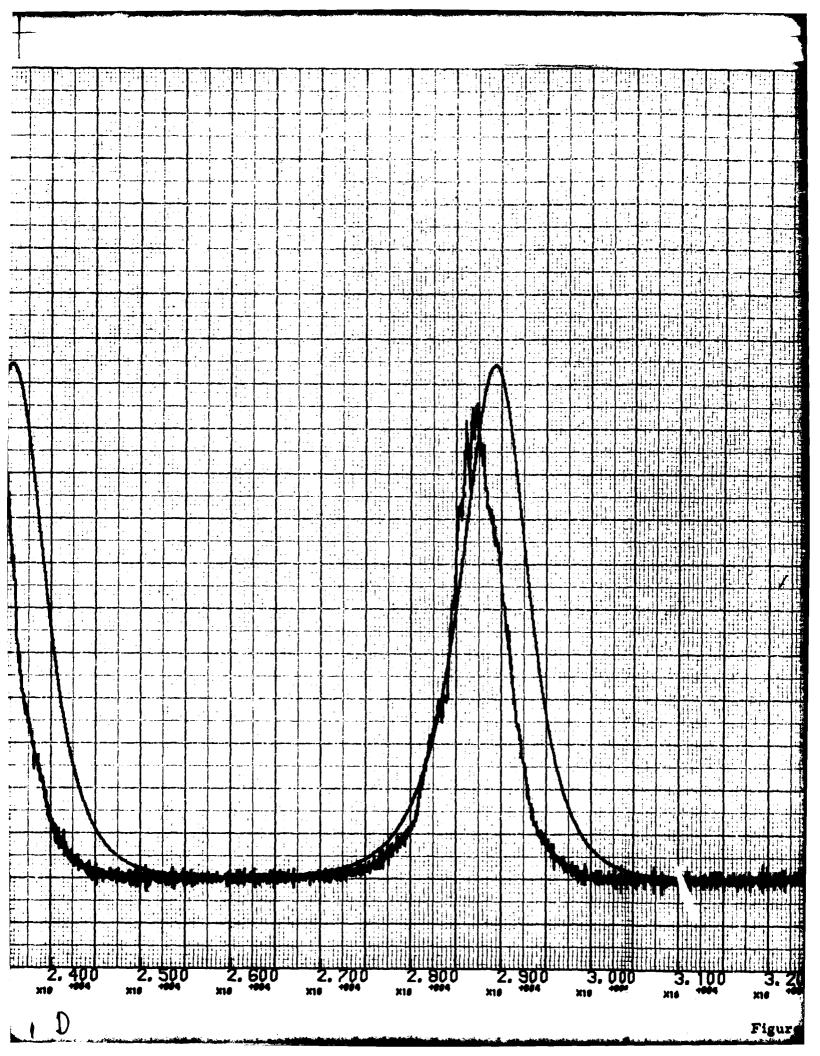
Figure V-1 shows a comparison of the model drag accelerations and the raw DMS sensed accelerations. It is readily seen that their amplitudes do not agree, nor do points of maximum drag in the two sets of acceleration profiles occur at the same time. Approximately 240 sec of data was dubbed on the front of the DMS data and a multiplier, determined by the ratio of the total time spans, was then applied to the result to force alignment of the points of maximum drag. Since the orbital periods were very nearly equal, the multiplier was quite close to 1, specifically 0.99770736. This resulted in the situation depicted in Figure V-2.

If this data were used directly for real world drag acceleration without further scaling, it is possible that the resulting integrated real world ephemeris would have times of perigee passage out of phase with the times of maximum drag force. Also, the magnitude of the perigee drag acceleration itself might have appeared unreasonable in the absence of any scaling. To prevent this from occurring, the amplitude of the data was scaled so the real world energy loss would be the same as that of the model. Specifically, the energy loss is directly proportional to the velocity loss

$$\Delta V = \int a_D dt$$

where  $\mathbf{a}_{\mathbf{D}}$  is the drag acceleration.





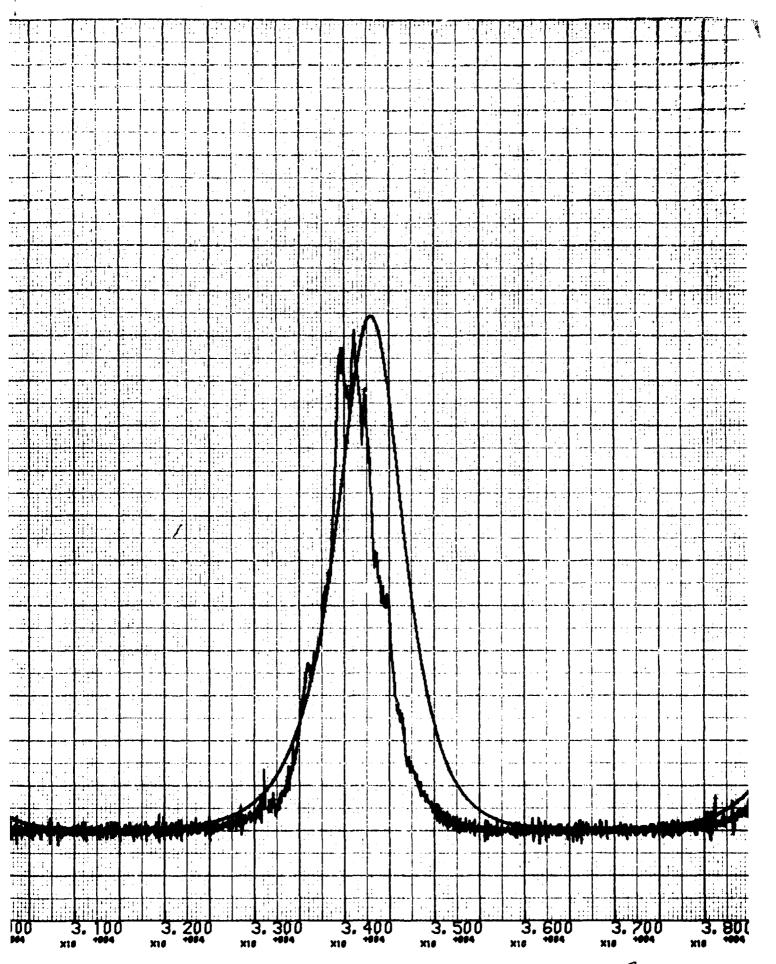
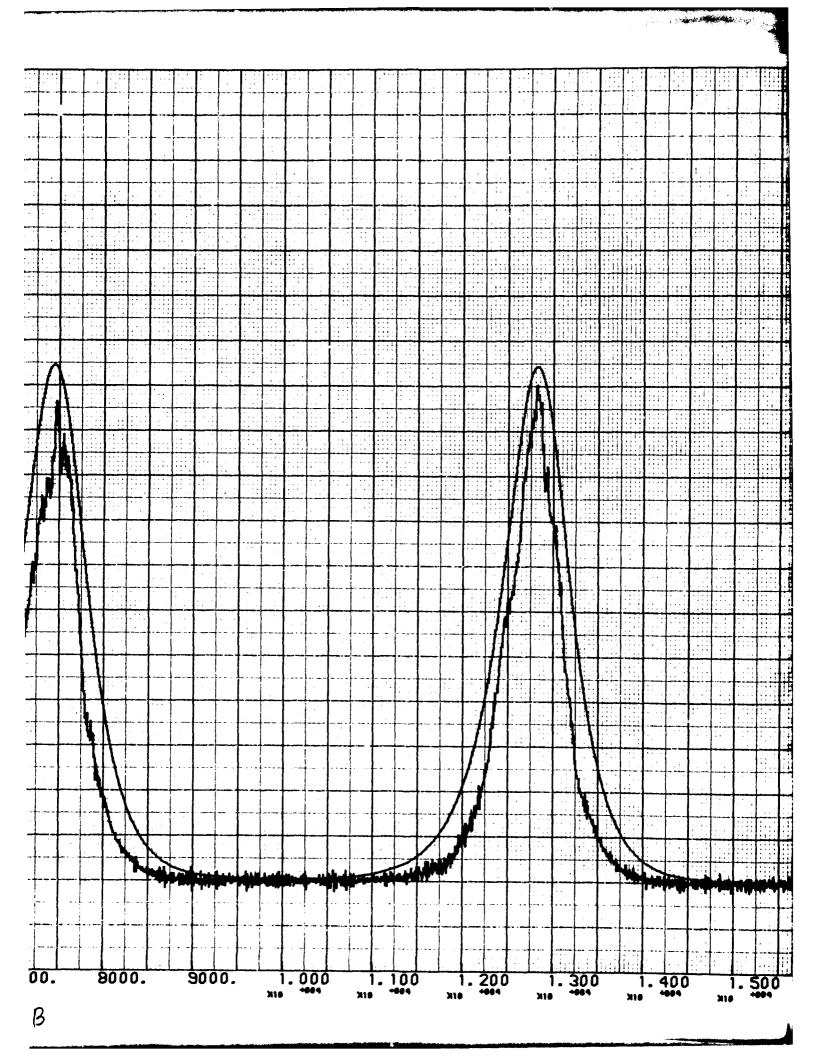
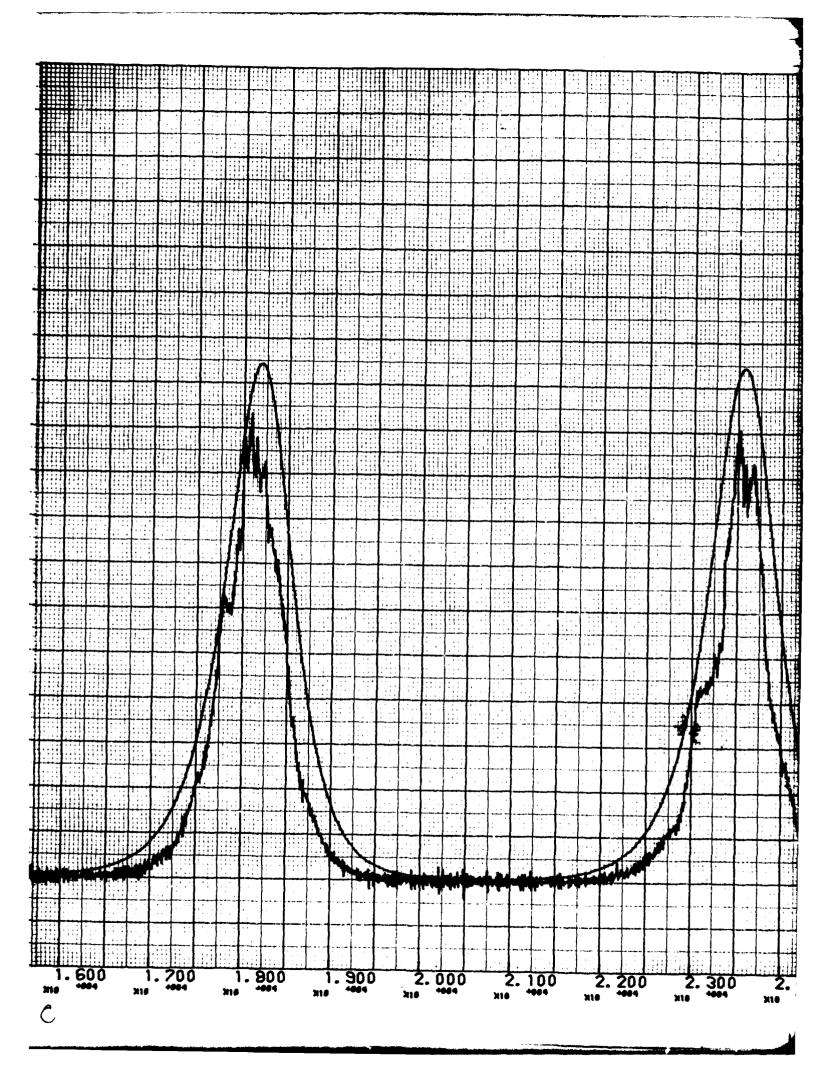


Figure V-1. Raw DMS Data and "Model" Drag Data

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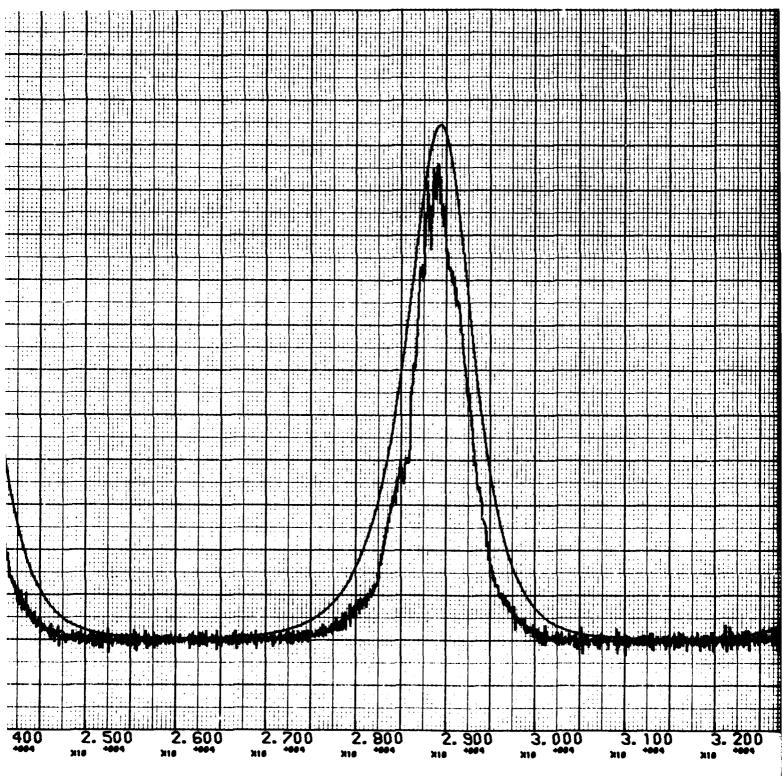
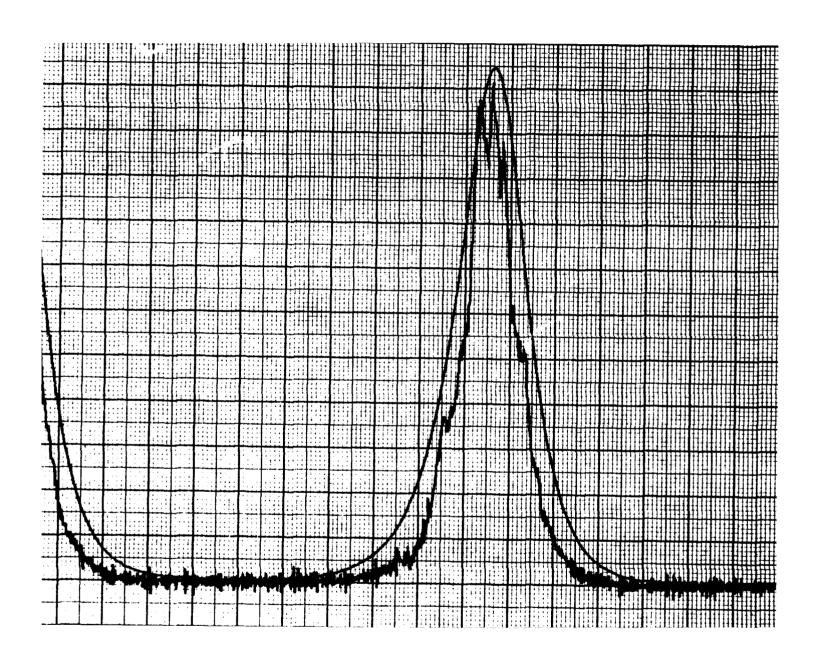


Figure V-2. DMS D



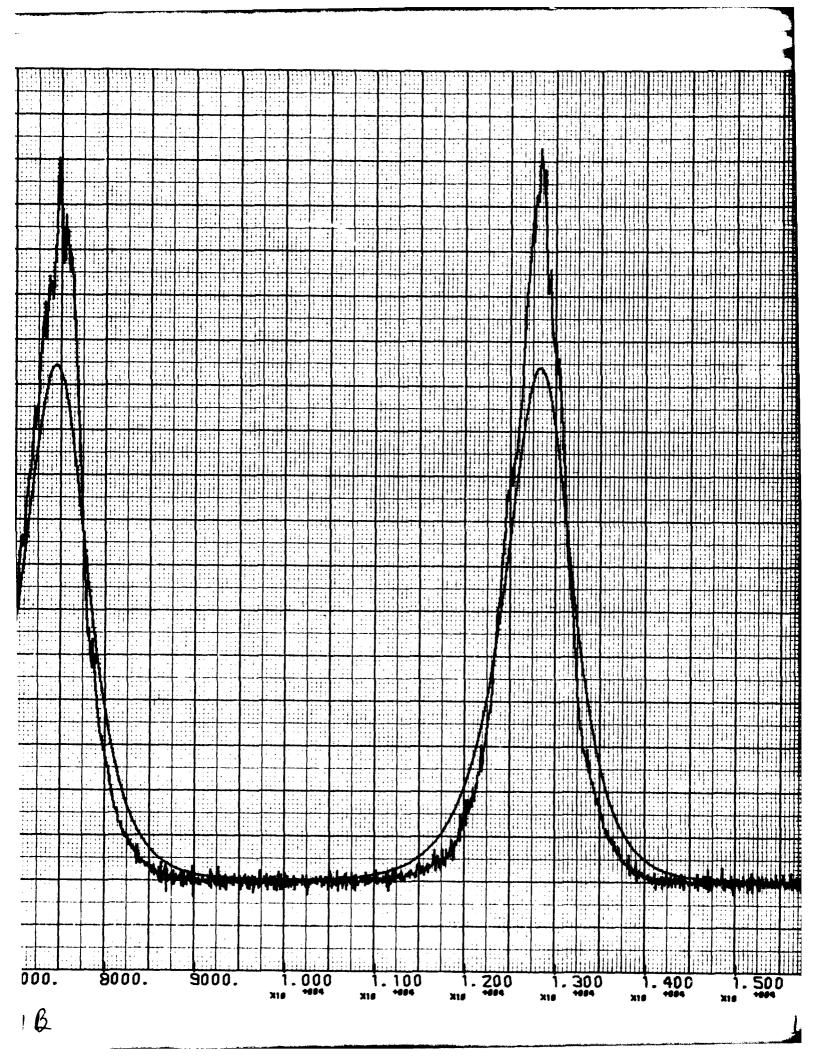
The accelerometer data scaling was done two different ways. In the generation of the real world atmosphere data reported on herein, the energy loss, or  $\Delta V$ , was preserved on a rev-to-rev basis. A second candidate real world ephemeris was also generated in which the total 20-rev  $\Delta V$  was preserved instead.

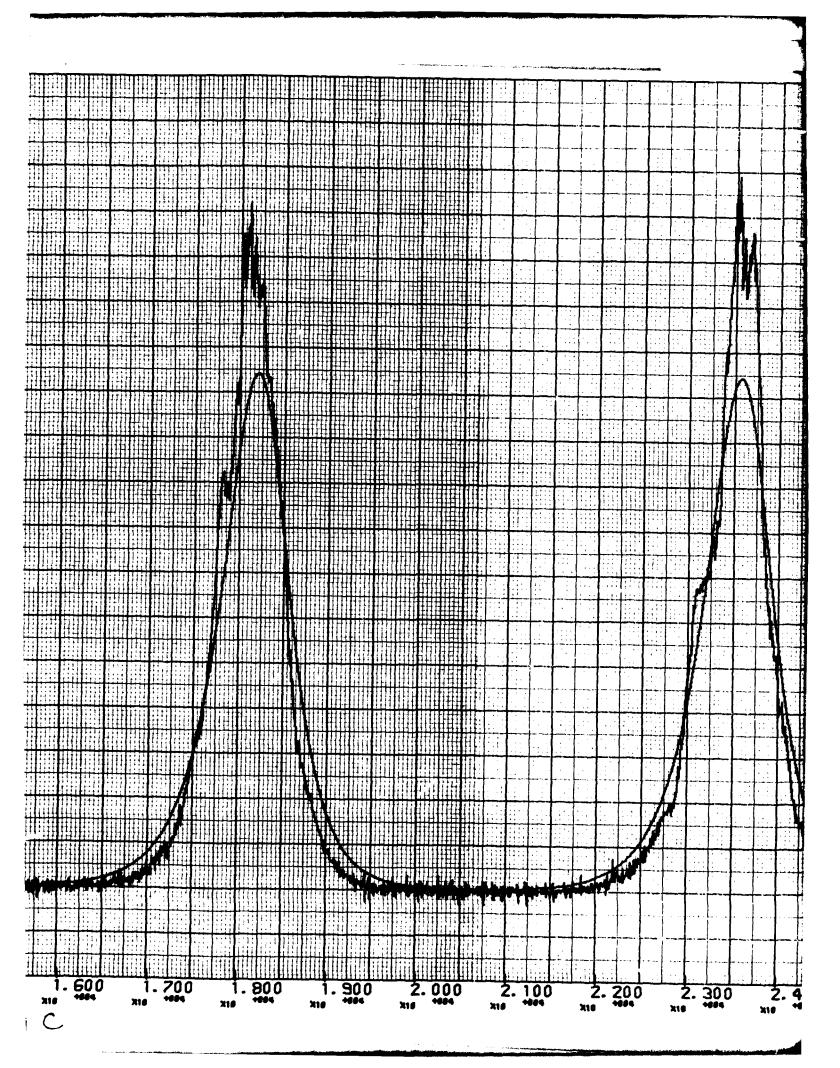
The slight differences between the two real world ephemerides using rev-to-rev  $\Delta V$  scaling and 20-rev  $\Delta V$  scaling were considered negligible and the former case was chosen, albeit somewhat arbitrarily, to be the real world drag profile for this study. Although the DMS vehicle's perigee was about 73 n mi, it had a lower ballistic coefficient (0.008 ft<sup>2</sup>/lb) than that chosen for the reference vehicle (0.02 ft<sup>2</sup>/lb). As a result, the rev-by-rev velocity loss for the DMS flight was less than that for the reference orbit. Each rev of the DMS data was scaled by the ratio

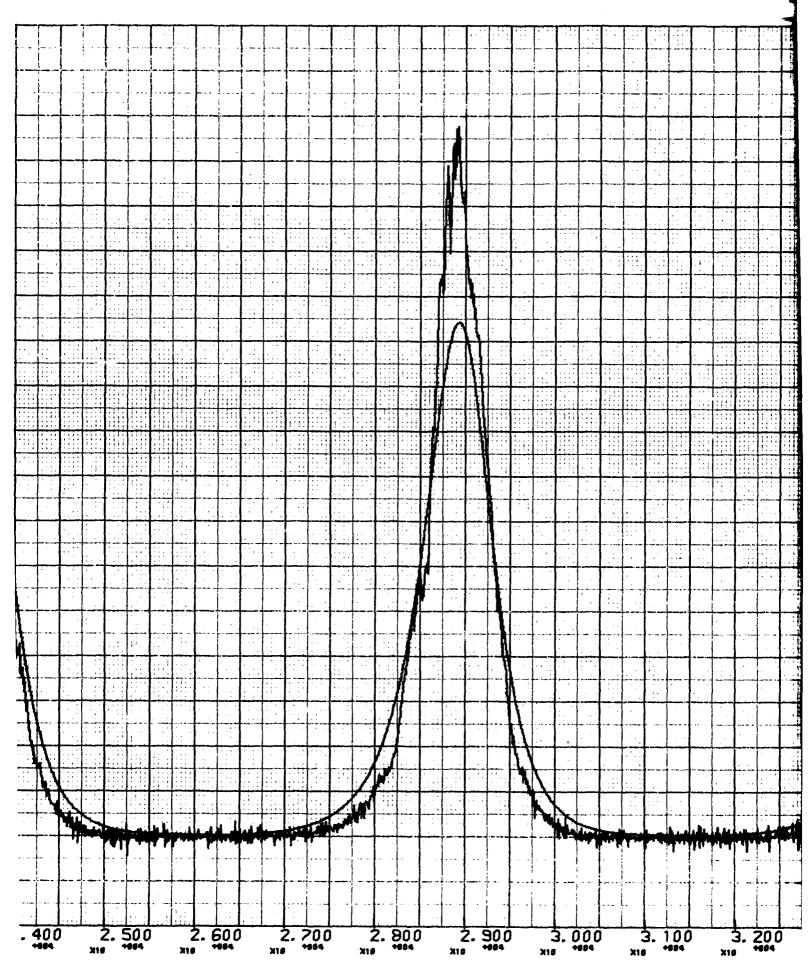
# $\frac{\Delta V \text{ loss reference}}{\Delta V \text{ loss DMS}}$

which is a number greater than 1. Figure V-3 compares the now-normalized DMS data with the model drag profile. Each rev of both orbits imparts the same energy loss to the vehicle, but the real world drag at any given point within a rev generally differs from that of the model. As Figure V-3 shows, it would be extremely difficult to reproduce the normalized DMS acceleration profile with an atmosphere model.

The normalized DMS drag profile was written on tape in a format suitable for use as an accelerometer input to TRACE.







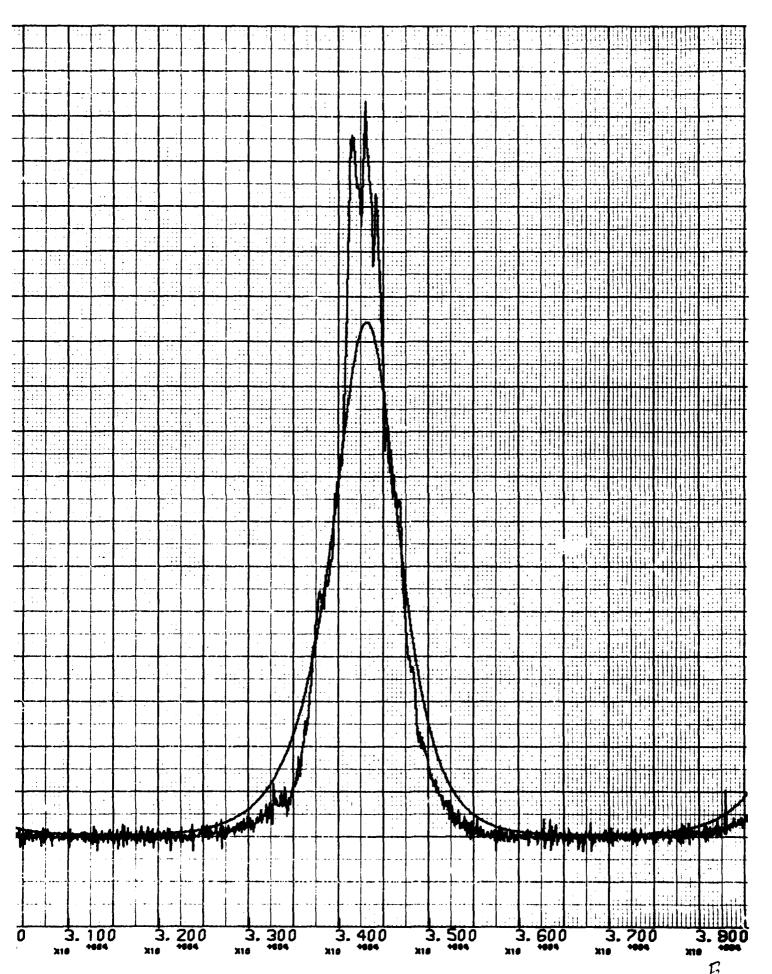


Figure V-3. DMS Data; Scaled Rev-by-Rev

## SECTION VI

### "REAL WORLD" EPHEMERIS

The geopotential described in Section IV and the accelerometer drag profile described in Section V were used as force models together with the initial conditions described in Section II. The gravitational attractions of the sun and moon were also included to make the real world ephemeris as near to the real world as possible. The integration was carried out over the same 20 revs as the model case.

Since the real world drag impulse was forced to agree on a rev-to-rev basis with the model drag impulse, the nodal crossing times and positions for the real world ephemeris should be close to those of the model ephemeris. Table VI-1 contains (in the same format as Table II-2) these conditions for the real world ephemeris.

A computer listing of the ephemeris for the first two revs is included in Appendix B.

Table VI-1. Nodal Conditions for "Real World" Ephemeris

Node	Nodal Crossing Time (Mo/Day/Yr) (Hr/Min/Sec)	Position XYZ (ft)	Velocity XYZ (fps)  6.16441283E+3 6.00674669E+3 2.36312409E+4			
0	2/29/80 22/30/0.0	-1.59387495E+7 1.51831715E+7 3.84199432E-15				
1	2/29/80 23/59/34.86323	-1.59847865E+7 1.51293060E+7 -4.34333501E-4	6.14523022E+3 6.02755269E+3 2.36341645E+4			
2	3/1/80 1/29/9. <b>D</b> 7663	-1.60300679E+7 1.50750883E+7 -9.00100265E-4	6.12585377E+3 6.04795515E+3 2.36378708E+4			
3	3/1/80 2/58/42.47044	-1.60754250E+7 1.50202680E+7 -3.72571321E-4	6.10597427E+3 6.06962440E+3 2.36415889E+4			
4	3/1/80 4/28/15.08251	-1.61214667E+7 1.49650787E+7 7.13800964E-5	6.08564728E+3 6.09052957E+3 2.36449662E+4			
5	3/1/80 5/57/47.03614	-1.61672548E+7 1.49094396E+7 -1.45264228E-3	6.06617102E+3 6.11093468E+3 2.36485783E+4			
6	3/1/80 7/27/18.19338	-1.62122626E+7 1.48540354E+7 2.97112782E-5	6.04648130E+3 6.13218703E+3 2.36522571E+4			
7	3/1/80 8/56/48.50253	-1.62571392E+7 1.47988953E+7 -1.44689247E-3	6.02720411E+3 6.15384146E+3 2.36551901E+4			
8	3/1/80 10/26/17.98143	-1.63017930E+7 1.47434625E+7 -9.23928079E-5	6.00754997E+3 6.17519473E+3 2.36584412E+4			
9	3/1/80 11/55/46.64434	-1.63463189E+7 1.46883472E+7 -1.65842335E-3	5.98752310E+3 6.19610495E+3 2.36615671E+4			

Table VI-1. Nodal Conditions for "Real World" Ephemeris (Continued)

Node	Nodal Crossing Time (Mo/Day/Yr) (Hr/Min/Sec)	Position XYZ (ft)	Velocity XYZ (fps)
10	3/1/80 13/25/14.56680	-1.63910809E+7 1.46329058E+7 -3.17691850E-4	5.96715899E+3 6.21640000E+3 2.36645896E+4
11	3/1/80 14/54/41.66063	-1.64355506E+7 1.45773503E+7 -2.74429165E-4	5.94617177E+3 6.23661260E+3 2.36677299E+4
12	3/1/80 16/24/8.03161	-1.64803676E+7 1.45214059E+7 -1.76019997E-3	5.92479582E+3 6.25703989E+3 2.36702724E+4
13	3/1/80 17/53/33.60059	-1.65248092E+7 1.44654088E+7 1.48863718E-4	5.90404820E+3 6.27813694E+3 2.36727759E+4
14	3/1/80 19/22/58.32904	-1.65687151E+7 1.44090721E+7 2.95331619E-6	5.88415436E+3 6.29922478E+3 2.36757447E+4
15	3/1/80 20/52/22.17168	-1.66122750E+7 1.43525901E+7 -2.52707804E-4	5.86433410E+3 6.32034803E+3 2.36787538E+4
16	3/1/80 22/21/45.07135	-1.66551805E+7 1.42959754E+7 -9.01314653E-4	5.84432969E+3 6.34130557E+3 2.36821387E+4
17	3/1/80 23/51/7.11635	-1.66982314E+7 1.42396118E+7 -1.36532782E-3	5,82390063E+3 6,36152469E+3 2,36851197E+4
18	3/2/80 1/20/28.39917	-1.67405388E+7 1.41829899E+7 -1.23762579E-3	5.80307017E+3 6.38107658E+3 2.36889368E+4
19	3/2/80 2/49/48.79290	-1.67827649E+7 1.41258533E+7 -9.02900611E-4	5.78157663E1+3 6.40182983E1+3 2.36928140E1+4
20	3/2/80 4/19/8.28148	-1.68255872E+7 1.40682145E+7 -9.47885195E-4	5.75967552E+3 6.42207719E+3 2.36964598E+4

## SECTION VII

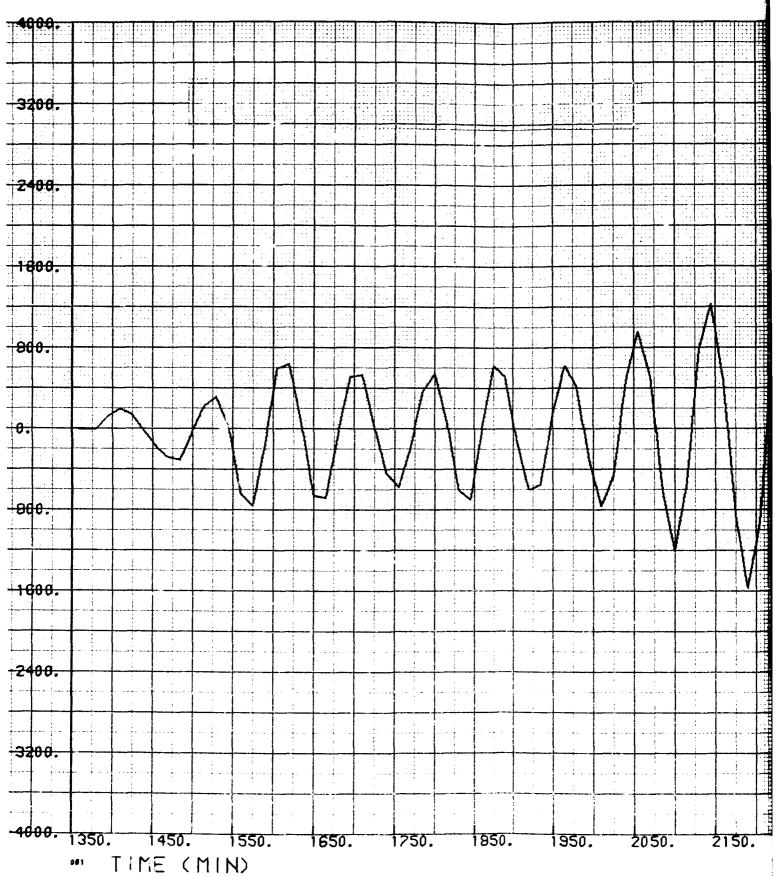
#### COMPARISONS OF "MODEL" AND "REAL WORLD" EPHEMERIDES

A trajectory difference run, similar to those described in Section IV, was made for the model and the real world ephemerides. Figures VII-1a, b, and c depict the radial, in-track, and cross-track differences, respectively. The radial difference plot shows a 1-rev periodicity whose amplitude grows with time to approximately 3300 ft by rev 20. The in-track difference plot also shows a 1-rev periodicity with maximum amplitude about 5000 ft and a secular term which grows about 750 ft/rev. Much of this secular growth can be attributed to the differences in GM between the two geopotentials (the model GM is 1.4076538841E+16 ft \$\frac{3}{3}\$/sec\$, while the real world GM is 1.4076468597E+16 ft \$\frac{3}{3}\$/sec\$. The cross-track difference plot shows a clear 1-rev periodicity and modulation at some multiple number of revs. The maximum amplitude is about 800 ft; no secular growth is discernible.

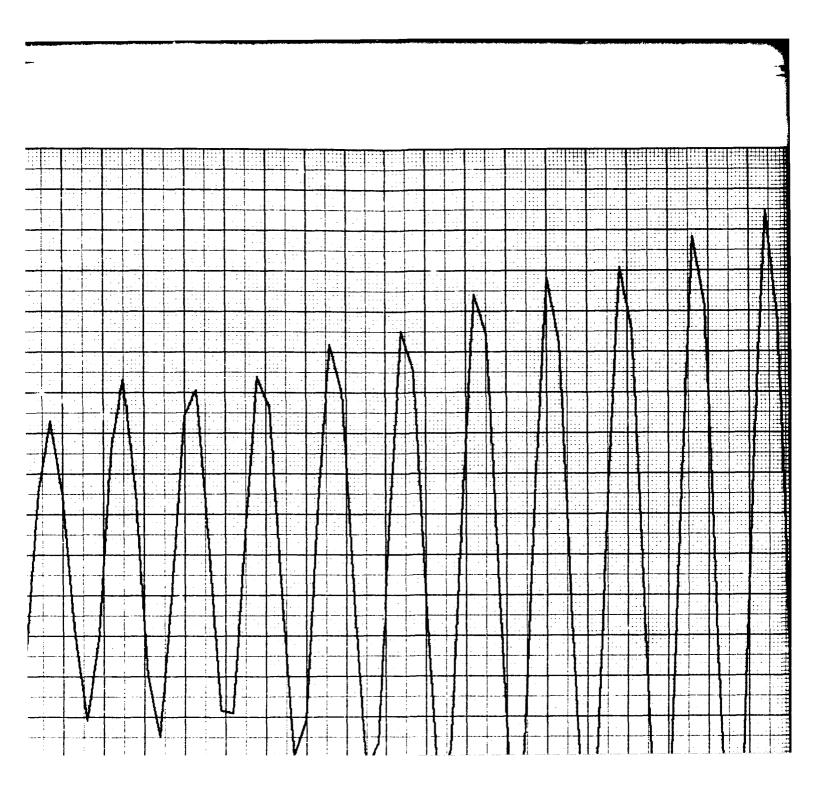
To further illustrate the differences between the model and real world ephemerides, the latitude, longitude, and altitude at selected perigees throughout the 20-rev span are shown in Table VII-1.

From the foregoing, it is reasonable to conclude that the real world ephemeris is in a sense representative of the real world. It is probably not as complex as the actual real world, but it is sufficiently more complex than an ephemeris generated by conventional models for the purpose at hand. The difference run just discussed indicates that the real world ephemeris could not readily be reproduced by conventional modeling techniques.

The content and format of the final data tape delivered to contractors is discussed in Appendix C.



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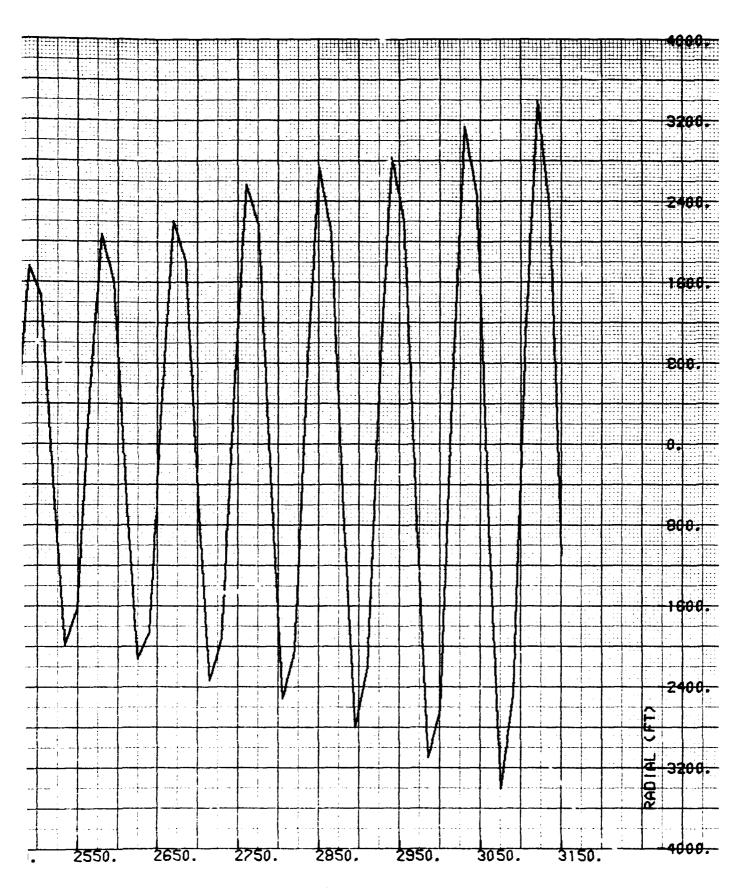
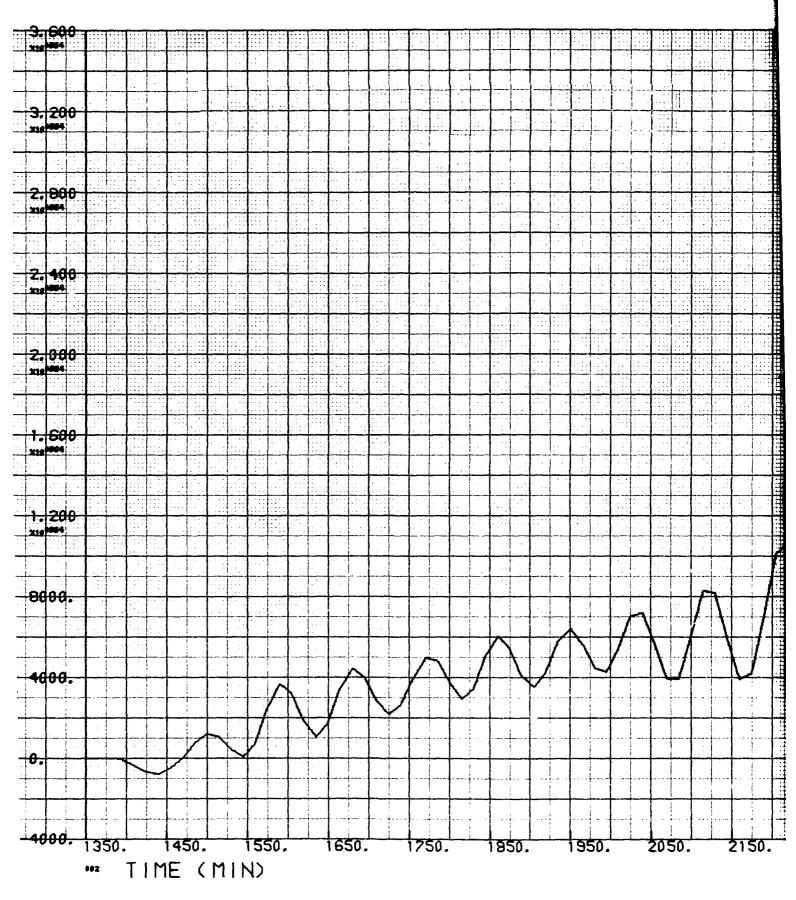


Figure VII-ia. Radial Difference Between "Model" Ephemeris and "Real World" Ephemeris



H

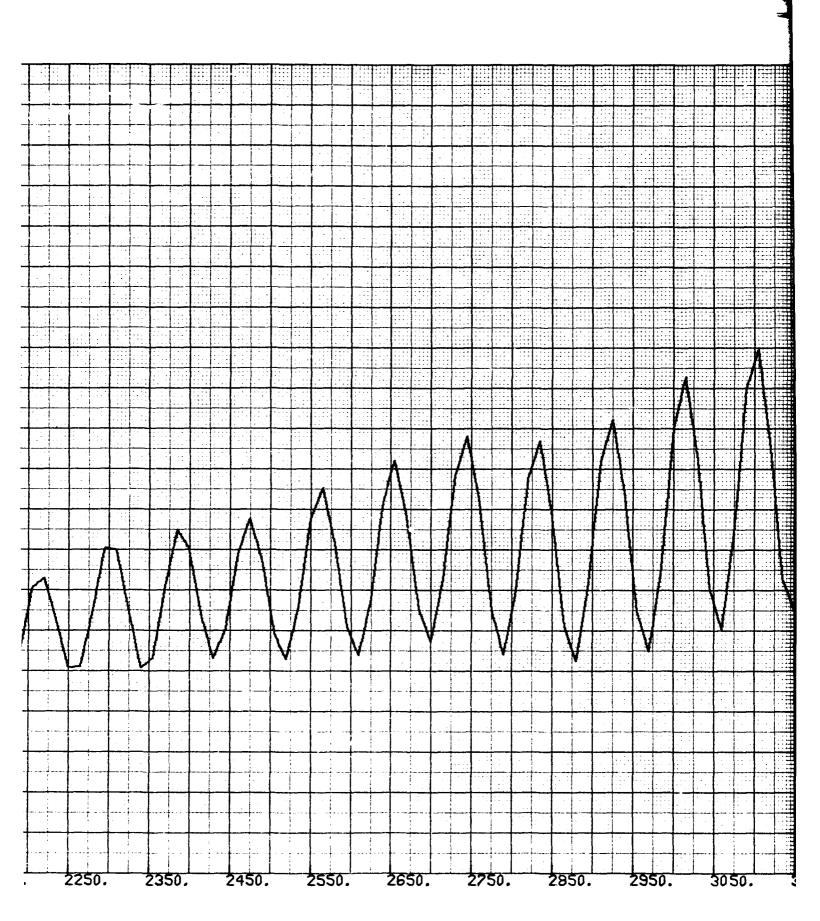


Figure VII-ib. Intrack Difference Between "Model" Ephen and "Real World" Ephemeris

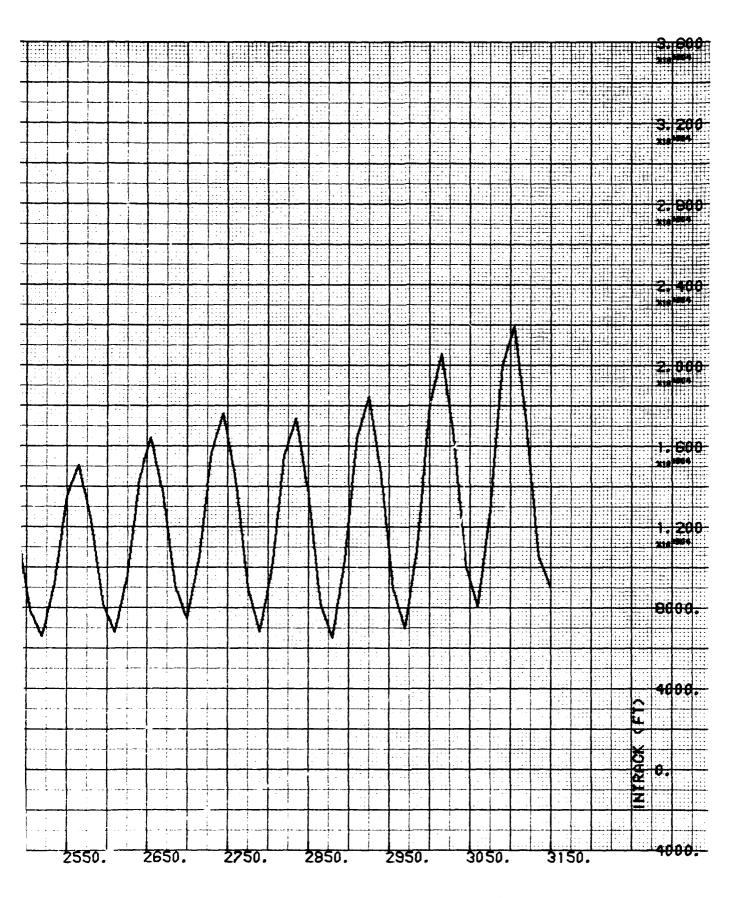
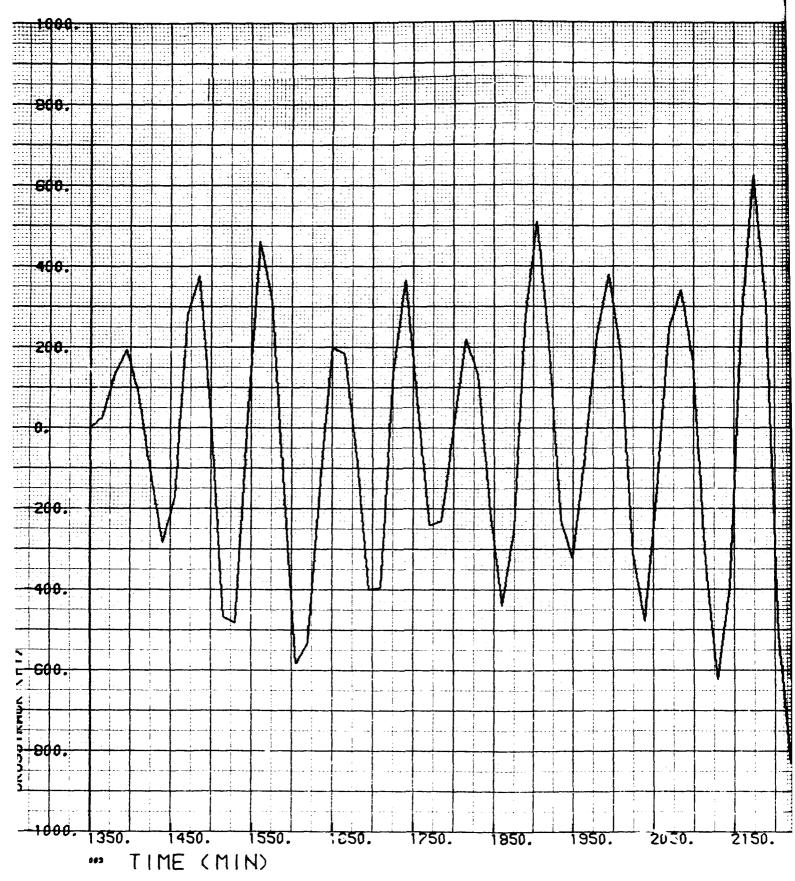


Figure VII-ib. Intrack Difference Between "Model" Ephemeris and "Real World" Ephemeris



A

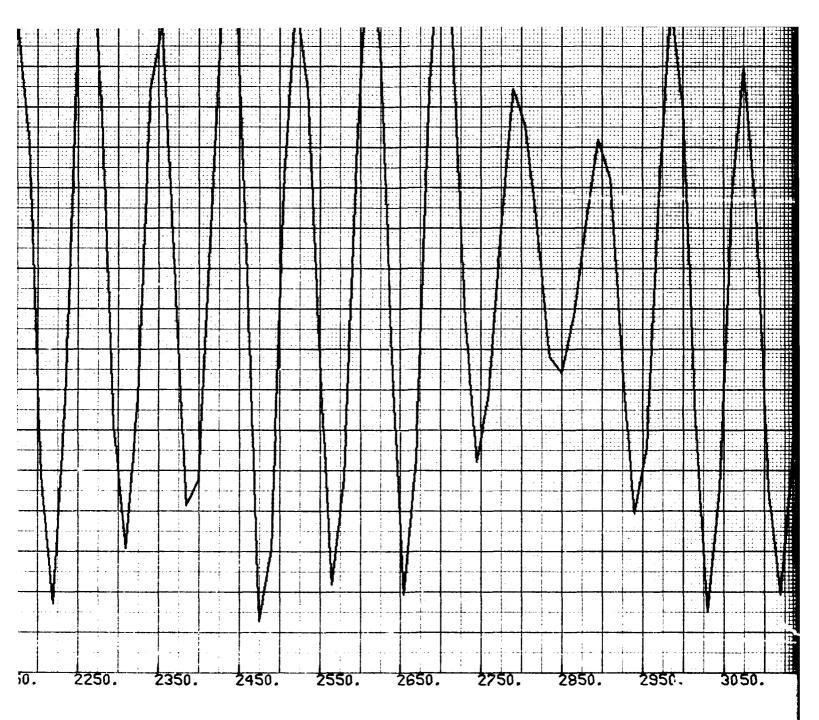


Figure VII-ic. Crosstrack Difference Between "Model" Ephemeris and "Real World" Ephemeris

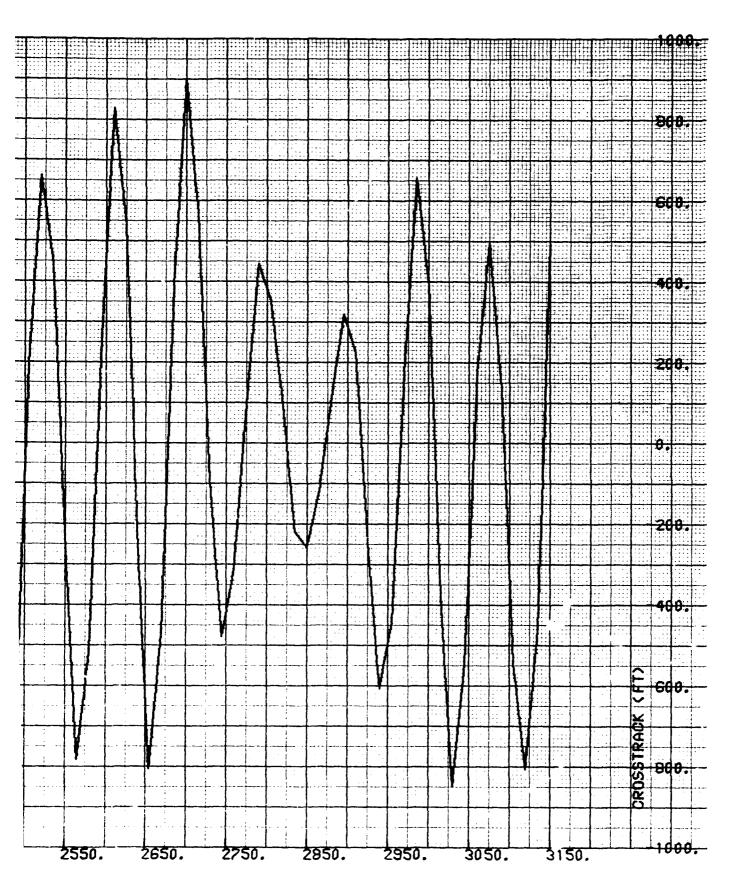


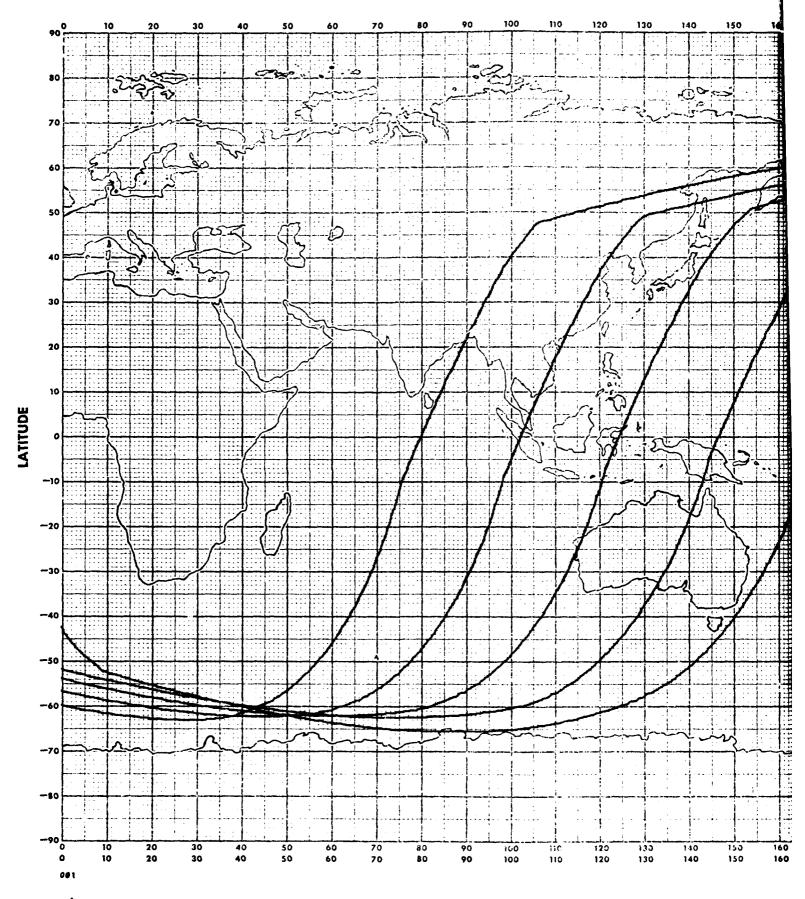
Figure VII-ic. Crosstrack Difference Between "Model" Ephemeris and "Real World" Ephemeris

Table VII-1. Selected Perigees from "Model" and "Real World" Ephemerides

Perigee		''Model''	''R	teal World"
1	LAT	45.17868651°	LAT	45.16178965°
	LONG	193.33637181°	LONG	193.32125882°
	ALT	81.36217 n mi	ALT	81.36947 n mi
5	LAT	45.67476127°	LAT	45.72686973°
	LONG	104.69701390°	LONG	104.74014037°
	ALT	81.36473 n mi	ALT	81,46199 n mi
10	LAT	46.38336256°	LAT	46.44256510°
	LONG	354.06792672°	LONG	354.11780809°
	ALT	81.16635 n mi	ALT	81.44194 n mi
15	LAT	46.83655544°	LAT	46.785755642
	LONG	243.30253604°	LONG	243.25405421°
	ALT	80.79841 n mi	A1.1	81, 16392 n mi
20	LAT	47.48427983°	LAT	47.43200754°
	LONG	132, 81690727°	LONG	132.76370666°
	ALT	80.54562 n mi	T.IA	81, 12460 n mi

## APPENDIX A

GROUND TRACE OF THE "MODEL" EPHEMERIS



μ-

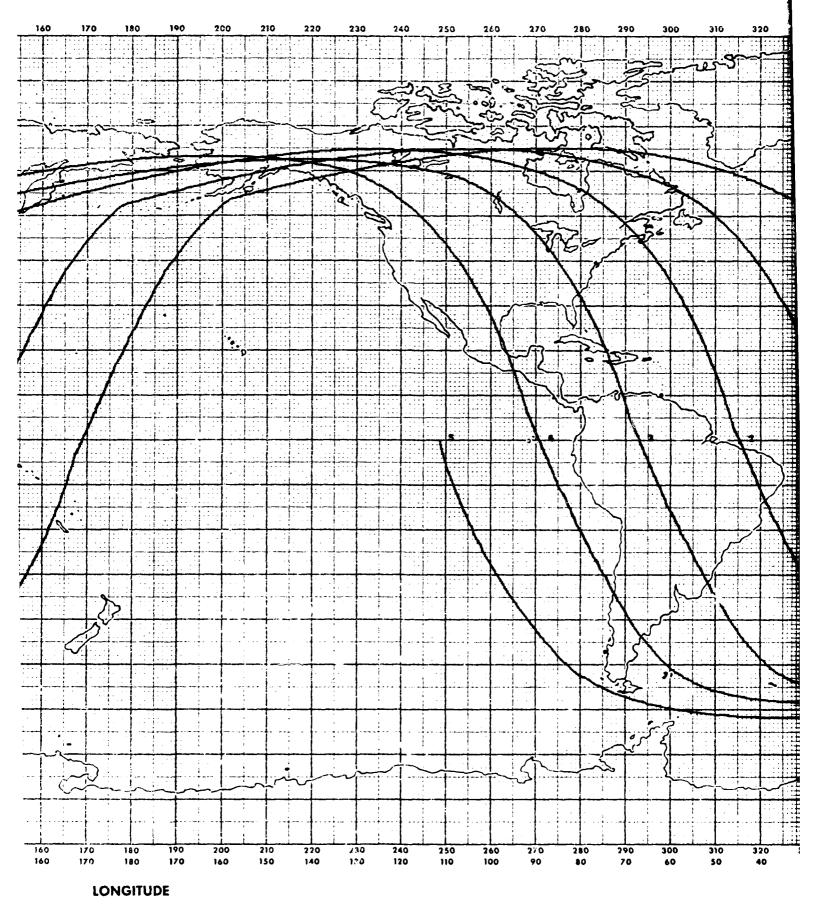


Figure A-1. Ground Trace, Revs 1 through 5

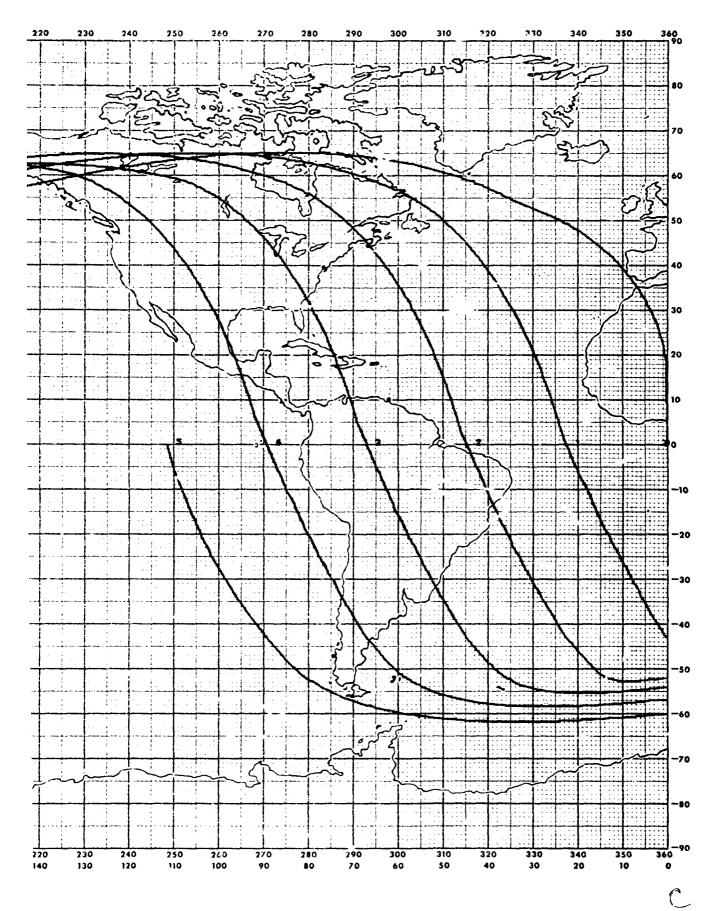
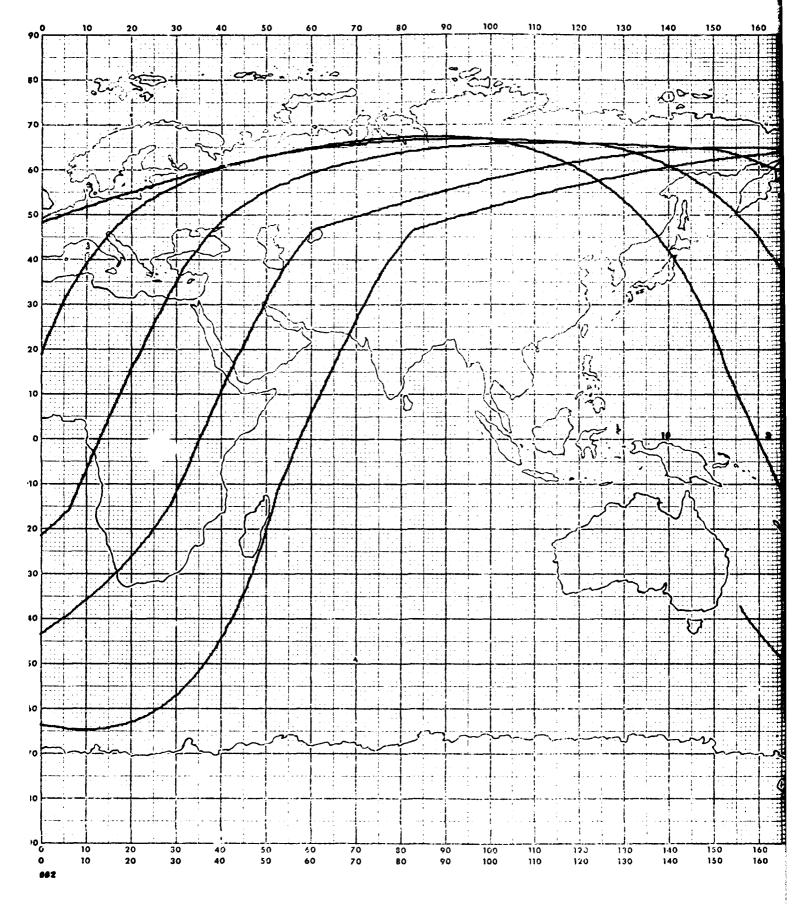


Figure A-1. Ground Trace, Revs 1 through 5



A

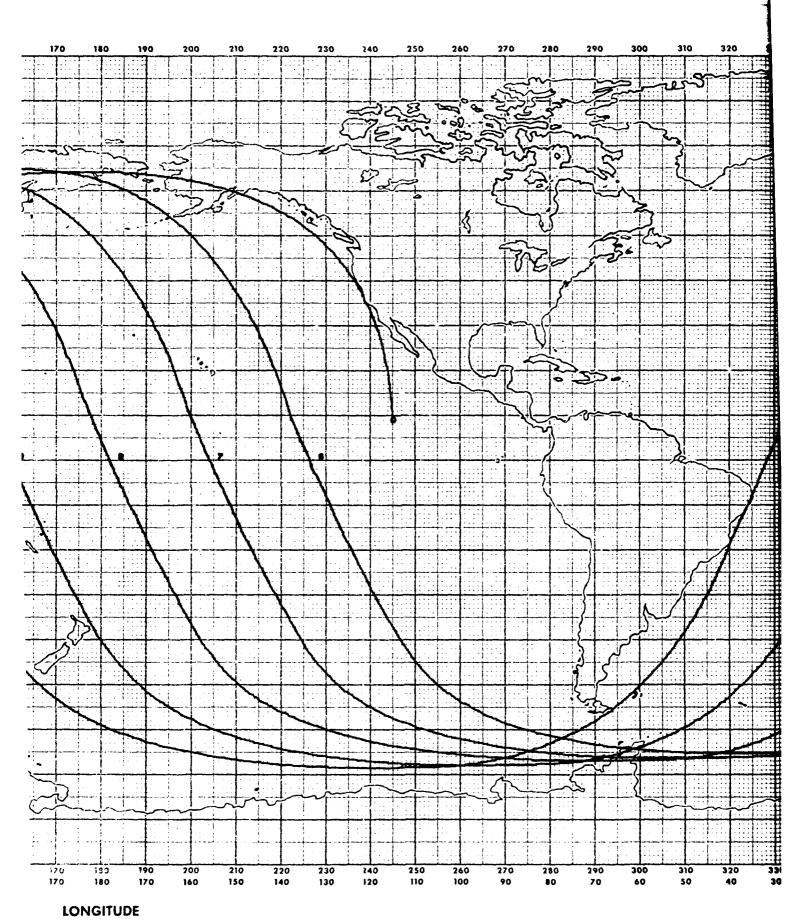


Figure A-2. Ground Trace, Revs 6 through 10

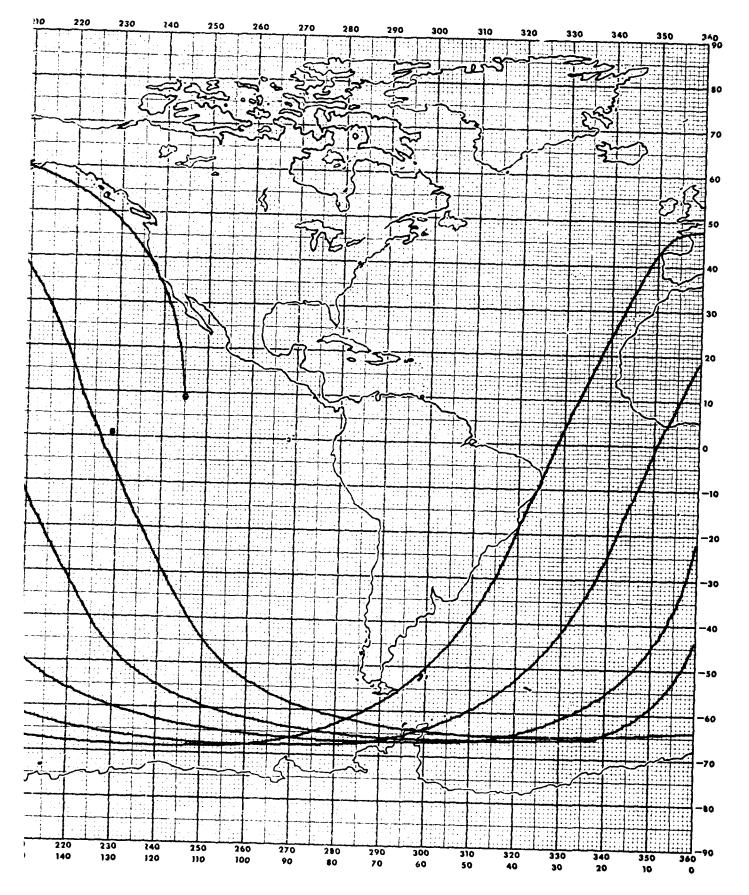


Figure A-2. Ground Trace, Revs 6 through 10

A

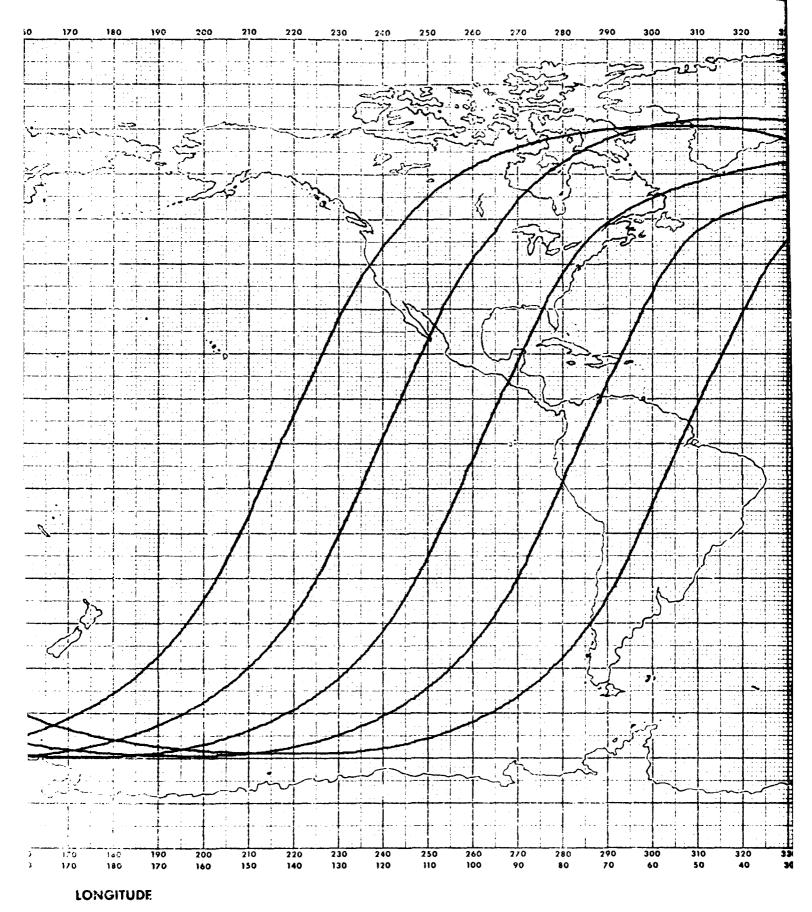


Figure A-3. Ground Trace, Revs 11 through 15

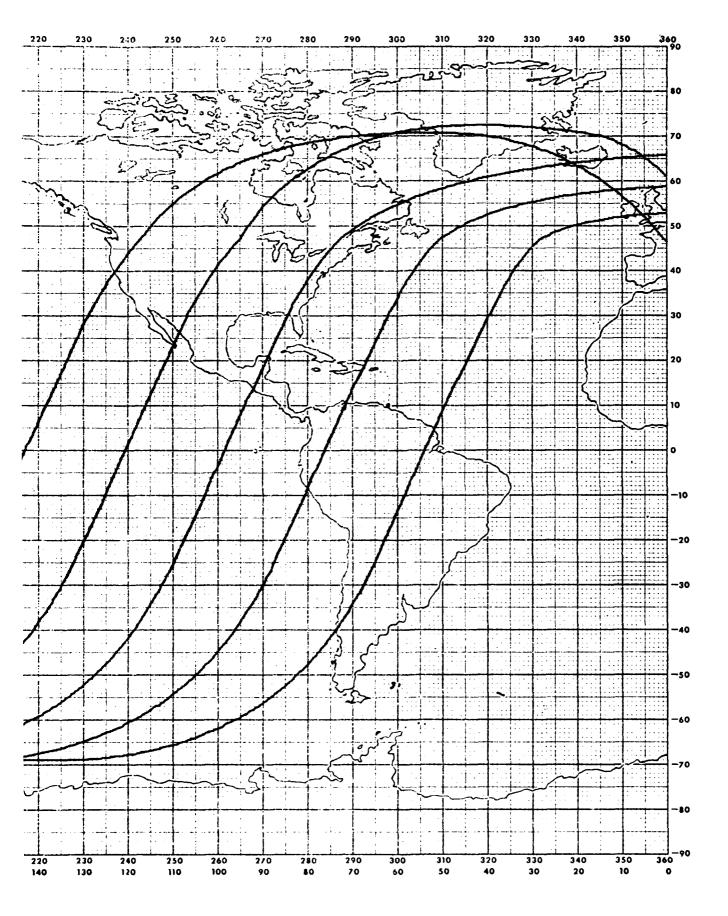
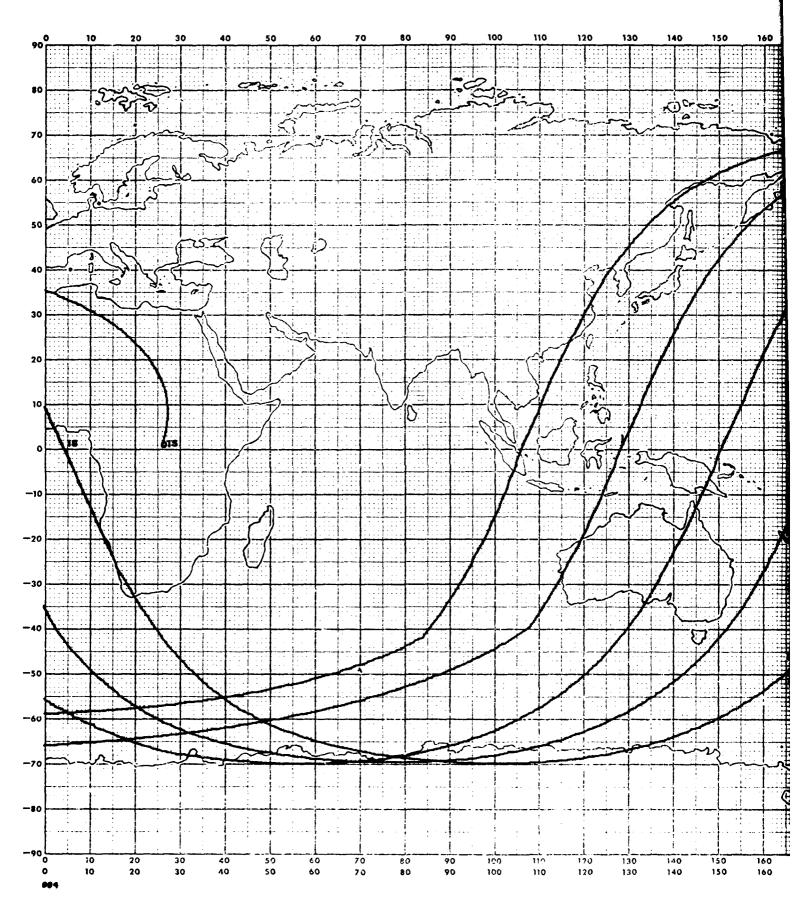


Figure A-3. Ground Trace. Revs 11 through 15



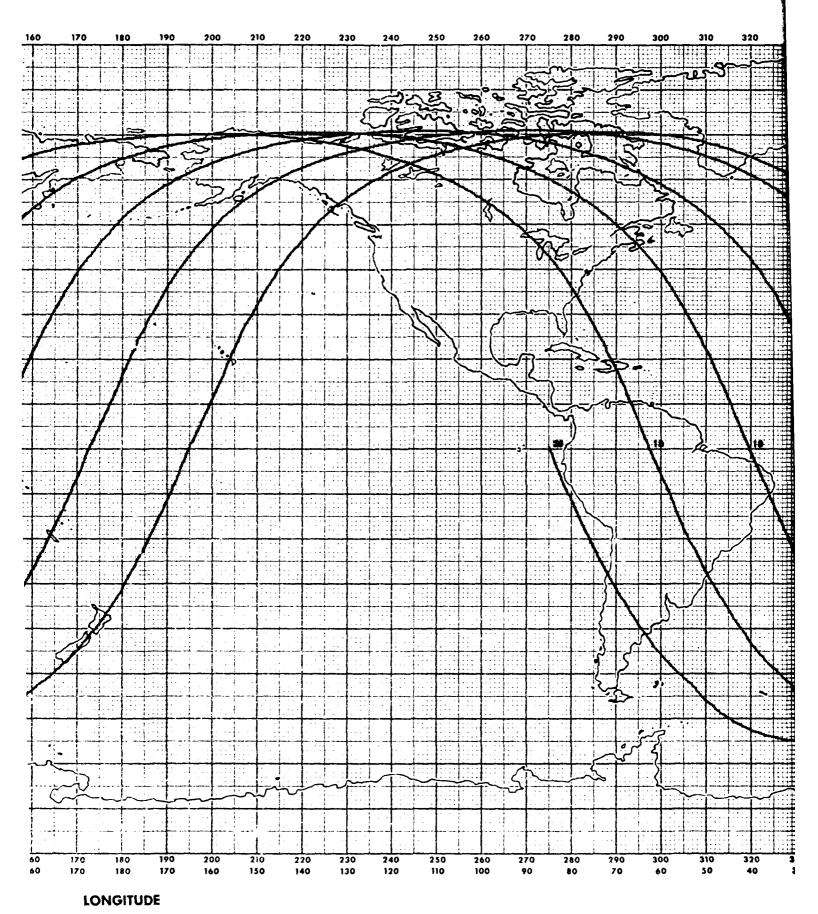


Figure A-4. Ground Trace, Revs 16 through 20

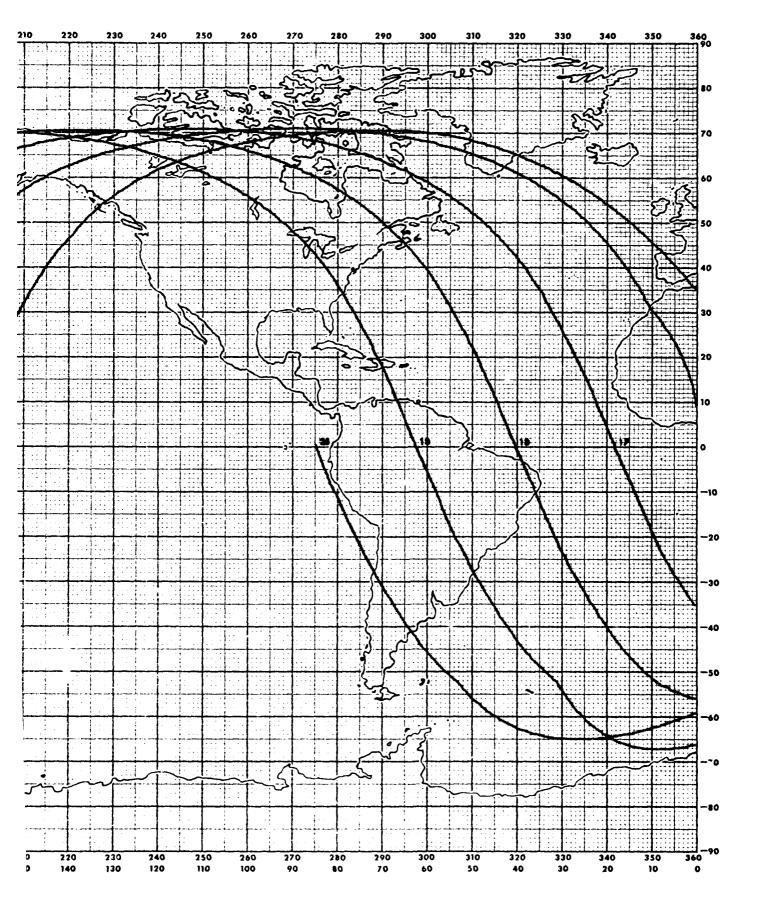


Figure A-4. Ground Trace, Revs 16 through 20

## APPENDIX B

TIME HISTORY OF "REAL WORLD" EPHEMERIS;
REVS 0 THROUGH 2

0.016	15,4M,ST,01	X,Y,Z,R	9x, 0Y, 0Z, V	LAT,	ALPHA,	REV	RE MARKS
MOZDAY/YR HOZHIN SEC	AIN FOOM	X (FT) Y (FT) Q (FT)	0x (FT/SEC) 0y (FT/SEC) 0x (FT/SEC) v (FT/SEC)	LATITUDE (DEG) LONGITUDE(DEG) ALTITUDE (NM) S-JEH-LAT(DEG)	ALPHA (DEG) DELTA (DEG) RETA (DEG) AZIMUTH(DEG)	REV COUNT PERTOD PER-DECAY NOD-REG	
		*		S TANK TO SECTION OF THE SECTION OF			
		* C APOGEE * O MIN ANI * K KEPLER	SPECIAL DIFFIL OF SPECIAL BADGEE PERIGEE MIN AND WAX METGHT ABOKEPLERIAN ELEMENTS VAGIATIONAL ED'ATIONS	SPECIAL OJEJJ OFIJJAS KTJOEJICO ADOGEE-PERIGEE MIN AND MAX METSHT ABOVE THE DALATE EARTH KEPLERIAN ELEMENTS VAPIATIONAL EDJATIONS	* * * * * * * * *		
		# # # # # #		*	• •		

ECT TRAJESTORY

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136.39075374 00000000 30.72980142 339.99949959 3.64.39396603 2.058171305402 3.523962385402 3.523962385402 3.523962385402 1.799958635400	ALPHA, 136.39075374 .00000000 90.72980142 339.99999959	1.4890507074E+11 -7.8816167744E+04	-5.8673251967E+08 9.6410262251E+03	3.643939AGE+03 2.05817130E+02 3.5239623E+03 8.5939619EE+01 -2.96605943E+00 1.79995963E+00
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1.593874955+07 1.51831715E+07 3.84199432E-15 2.201300595+07 ECCENTAIN FRUE ANDM = KEPL PER ANOM PER =	PRINTS X,Y,Z,R -1.59387495E+07 1.51931715E+07 3.84199432E-15 2.20130059E+07	VELDSITY PELATIVE TO SUN 445, x, y, z, 2, 4,8635421938E+11 445, x, y, z, 2,466735451E+04	1.3054905340E+09 2.708005353E+04	HEAN ANOM E EGGENTALO E 19UE ANOM E KEPL PER E ANOM PER E
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ALPHA 105.8A111937 54.34645179 90.95667154 324.03079754	1.4982567691E+11 -3.7124771743E+04	-5.8741090496E+08 -3.5588783781E+03	3.63861410E+03 1.99555786E+02 3.51527367E+03 7.62263580E+01 1.90737022E+00	345.53028160 53.12928216 90.16292021 214.78922008	1.4873399970E+11 -1.0335110202E+05	-5.0037484332E+09 -1.5876525467E+04	3.63437575E+03 1.9610884E+02 3.51944104E+03 A.11741263E+01 -2.98927426E+09 1.80750546E+00
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2 m V m V m V m V m V m V m V m V m V m	5.4503171677E+10 -5.2804921358E+04 -2.4554858353E+08 -1,5192812092E+04	02 01 01 00 00 000000 0.00000	1 11 0000000	00
ALPHA, 337.81077404 44.96935118 90.0000001	1.4871974196E+11 -1.0246393356E+05 -5.0251636123E+08 -1.4988023199E+04 S4 = 1.60491274E+	3.63734934E+03 1.99214131E+02 3.51951034E+03 8.13791281E+01 -2.96422584E+00 1.80594915E+00 1.80594915E+00 332.00623446 36.32215159 89.93736047	1.4870549495E+11 -1.3107402889E+05 -5.0452198967E+08 -1.3595770253E+08 -1.3595770253E+08 -1.3595770253E+08 -1.3595770253E+08 -1.3595770253E+08 -1.3595770253E+08 -1.3595770253E+08 -1.3595770253E+08 -1.3595770253E+08 -1.3595770252496E+08 -1.35957702524968E+08 -1.35957888805E+08	1.80428816E+00
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X+Y+2+R 1.4009059AE+17 1 -5.71391850E+17 -1 1.51133554E+17 -1 2.17849513E+17 2	TY RELATIVE TO SUN **2	MEAN ANOM : 3 ECCENTRIC : 3 TRUE ANOM = 3 KEPL PER : 8 ANOM DER : 8 NOOL PER : 8 X,Y,Z,Z 1,52175979E+07 7 -8,09921632E+05 -1 1,2569954E+07 -1 2,13901141E+07 -2	17 RELATIVE TO SUN 4.8632226984E+11 4.1849259279E+05 1.1849259279E+05 1.1849259279E+05 1.240108615E+09 1.340108615E+09 1.340108615E+09 1.340108615E+09 1.340108615E+09 1.340108615E+09 1.340108615E+09 1.340108615E+09 1.340108615E+09 1.34010861 1	PER :
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-4.59/34328225+11 1.4865073612E+11 5.4462077735E+10 -3.99/9697172E+04 -3.1442581075E+04 -5.0978029529E+04
1.1719378135E+09 -5.0974500373E+08 -2.6108011406E+08 -4.2159465191E+03 -3.9598707059E+03 -2.3362958985E+04
4.47562340E+01 APOSEE = 3.64674042E+03 4.50674453E+01 HEIGHT = 2.09079206E+02 4.57831379E+01 PERIGES = 3.52106038E+03 8.95922025E+01 HEIGHT = 8.23991604E+01 8.9552701E+01 0-001 = -2.96625059E+00 8.9580701E+01 U-001 = 1.80034723E+00
DX,DY,DZ,V LAT ALPHA, REV,7.039£1032£+03 -3.59135139 315,18262380 .51046 -5.42870/177;+03 167.51107305 -3.56737123 0.00000 -2.41347405;+04 -3.59067930 200.03981267 0.00000
-4,5953657658E+11 1.4864570148E+11 5.4458699751E+10 -4.1173437475E+04 -3.0267868143E+04 -5.0925525044E+04
1.1715705267E+09 -5.0993197812E+08 -?.6237374062E+08 -5.4261029778E+03 -2.7845246221E+03 -2.3310222172E+04
4.86169257E+01
95803503C+01 Dx, DY, DZ, V

43 .57477 80 0.00000 02 0.00000 57 0.00000	1 6.4408382612E+10 4 -4.738562479E+04	<b>∞</b> .≇	46+03 06+03 46+01 76+00 16+00	4E+03 4E+02 4E+01 7E+00 1E+00 1E+00 1E+00 1E+00 1E+00 1E+00 1E+00 1E+00 1E+00 1E+00 1E+00 1E+10 1E+00 1E+10 1E	+ + + + + + + + + + + + + + + + + + +
27 -57.91829080 53 89.10501902 19 220.13765457	1.4457307397E+11 -7.2079A2669E+04	-5.0382062473E+08 1.5412067561E+04	= 3.63760334E+03 = 1.99928924E+02 = 3.51445090E+03 = 7.67764894E+01 = -2.99236157E+00 = 1.80864841E+00	3 3 474	3 47 5 530
4 -59.09123173 4 129.52927127 4 16.32563 4 -54.0932679		2995+09 3955+04 APO36E HFIGHT		-52.02979 -52.02979 -52.02986 -52.02979 -52.02979	-52.03.86 -52.03.86 -52.03.86 -52.028.86 -52.028.86 -52.028.86 -52.028.86 -52.028.86 -52.028.86 -52.028.86 -52.028.86 -52.028.86
-1,90619502E+04 1,2764744E+04 -1,05934934E+04 2,52689530E+04	11 -4.5858032295E+11 05 -5.3183939591E+04	1.15009102995+0 04 -1.7454510395E+0 1.13999955F+02 At 1.14699955F+02 Hi	1.12777814E+01 9.93969049E+01 9.95488299E+01 8.95767125E+01	1.2795576+01 HF 9.95483796+01 HF 8.95767125E+01 U- 1.20213463E+04 -52. U 1.78023025E+04 -52. U 1.27905857E+04 -52. U	
2.21025035E+05 -1.14121226E+07 -1.854769146+07 2.18858497E+07	ITY RELATIVE TO SUN 17.2 4.863314929E+11 17.7 1.0133956455E+05		ARPL PER E NOOL PER E	PER	46+02 KEPL PEP = 9 2E+02 ANOM PER = 9 7E+03 NODL PGP = 8 7+03 NODL PGP = 8 7+03 NODL PGP = 8 7+04 NODL PGP = 8 7+05 X*Y,Z,Z 7+19131E+05 1 10000 -1.314736436+07 1 16557 2.21204973E+07 1 16557 2.21204973E+07 2 11Y RELATIVE TO 900N 1Y,Z 8.484955223E+04 1TY RELATIVE TO 900N 1Y,Z 1.315879459E+09 1Y,Z 2.6690502159E+04 5E-14 MGAN ANOM = 1
69.00000 1410.00000 84590.00090	VELOC MAS, X MAS, X	VELOCI MAD:*X: MAD:*X: 2393757 729353: 2191535	1.24693112E+02 1.39163127E+03	469312FE+03 916312FE+03 F5.00000 1425.00000 1425.00000 16557 VELOSITY REL 445;x,y,7	469312FE+03 469312FE+03 E,44,51,00 1625,0000 1625,0000 4657 VELOSITY REL MAS,x,Y,? MAS,x,Y,Y,? MAS,x,Y,Y,? MAS,x,Y,Y,? MAS,x,Y,Y,? MAS,x,Y,Y,? MAS,x,Y,Y,? MAS,x,Y,Y,? MAS,x,Y,Y,? MAS,x,Y,Y,Y,Y,Y,Y,Y,Y,Y,Y,Y,Y,Y,Y,Y,Y,Y,Y,
2729780 23730 0.00003	POSITION AND DISTANCE VELOCITY	STA	TAJ = 1	59790 29790 1955 1113N 7151A	• 0 0 2 + 0 2 + C

00000 0.00000 0.00000	6,4375663037E+10 -2,3294249313E+04	-2.7643965520E+08 1.4328718773E+04		REV97213 BETA =90 0.00000	5.4372695423E+10 -2.0470237778E+04 -2.7.35734196E+08 1.7153297675E+04		45V 450 NODE 1.00000 ASC NODE 0.1000
-50.12462705 89.84894975 327.72851112	1.4850971002E+11 (	5.4565533539E+08 -2.0288412126E+04	3.64171266E+03 2.03171632E+02 3.51334122E+03 7.48001929E+01 -2.98755928E+00	155.16292629 -42.40982236 39.9999995 332.34183482	1.4850052171E+11 -5.8175073975E+0% - -5.8296073238E+08 - 1.9327060949E+04	3.64175544F+03 2.03126791E+02 3.51593517E+03 7.7365174E+01 -2.98295829E+00 1.805626420	ALPHA, 136.57494797 000000000
7.09173262 203.90830 -50.30329592	•	• • •	APOSEE = HEISHT = PERIGES = HEISHT = O-001 = U-001 = E	LAT; -42.63057347 .17054077 293.11721 -42.67987998	च <b>्</b> ५	APOSEE = HEIGHT = PERISEE = HEIGHT = O-901 = U-331 = E	1 AT, 00100100 337.72761571
1.75377482E+04 1.350130A1E+04 2.49995712E+04	1 -4.5962784103E+11 4 -4.5576A15799E+04	9 1.1458544523E+0 4 -9.8713131215E+0	1.71601623E+02 1.71551669E+02 1.71701350E+02 8.94531516E+01 8.95503903E+01	0x,0Y,0Z,V 8.96412739E+03 1.66753113E+04 1.63255733E+04 2.49993841E+04	1 -4.5853385285.+11 4 -4.30563609255+04 9 1.1446813559E+09 4 -7.3643315044E+03	1.7999497E+02 1.7999997E+02 1.7999997E+02 A.95036245E+01 8.95507947E+01 8.95785972E+01	0x,0Y,0Z,V 6.145230?2E+U3 5.02755?69E+J3
4.28475955E+05 -1.69782728E+07 2.21232347E+07	Y RELATIVE TO SUN • 4.4635250520E+11 • 7.	Y RELATIVE TO MOON 1.3162157974E+09 1.2 2.5777799367E+04	MEAN ANON BECCENTACTO BETQUE ANOM BEQUE NOW BEQUE NOOL PER BECCENTACTOR BECCENTACTO	X,Y,Z,R -1.4911391E+07 - 6.61936421E+05 -1.49489412E+07 2.21277257E+07	TY RELATIVE TO SUN 4.2 4.853559853E+11 6.7 8.3196050324E+04 FY RELATIVE TO MOON 6.7 2.5970137412E+09	MEAN ANOM E ECCENTATO E TRUE ANOM E KEPL PEP E ANOM PER E	X,Y,Z,R -1.59847865E+07 1.51293069E+37
1425.53001 85531.80067 .16657	VELOCIT MAS+X+Y MAS+X+Y	VELOCIT MAG, X, Y MAG, X, Y	2.17374559E+07 1.79413659E+07 1.19017929E+02 1.35650356E+02 1.35650356E+02	MF,4M,3I,0I 77,79338 1427,79338 95657,60300	MASSXY, MASSXY, MASSXY, MASSXY, MASSXY,	2.55465537E-14 2.1765537E+07 1.10013845E+02 1.36556121E-02 1.36028417E+02 1.38304157E+33	4E,444,ST,DT 89.58195 1433.58105
23745	POSITION AND DISTANCE VELOCITY	0 N S T A L O C		2429/80 2729/80 23/47 47.5930	DISTA VELOS VELOS SITION VELOS VELOS		0ATE 2/29/80 23/59

34.95323	46374.463333 .16657	-4.34333915-04 2.20093002E+07	2,36341645E+04 2,51523113E+04	174.34217 99300300	90.72838080 340.00045711	0.00000
POSITION AND DISTANCE VELOCITY	TION AND VELOSITY REDISTANCE MAS, X, Y, 7 VELOSITY MAS, X, Y, 2	VELOJITY RELATIVE TO SUN MAG,X,Y,7 HAG,X,Y,7 8.4663699378E+UL	1 -4.59559050750+114 -2.79438485805+04		1.4944901842E+11 -7.9827679834E+04	5.4351519428E+10 -1.3133587897E+04
POSITION AND DISTANCE VELOCITY	VELOCITY MAS, K, Y, Z MAS, K, Y, Z	QELATIVE TO MOON 1.3054544339E+03 2.7097011136E+04	3 1.1447377124E+03 4 7.7430889770E+03		-;.7257479755E+D8 9.6912267524E+D3	2,5882374803E+08 2,4452900421E+04
	2.1743925E-14 2.17743925E+07 1.6673740EF-02 1.35574348E+02 1.31046916E+02	MEAN ANOM BECCENTALS BECCENTALS BECCENTALS BEAN BEAN ANOM BEAN BEAN BEAN BEAN BEAN BEAN BEAN BEAN	2,30405954E+02 2,29677536E+02 2,28953144E+02 8,959767959913185E+01	APOGEE = HEIGHT = PERIGES = HFIGHT = O-DOT	3.64335094E+03 2.05251441E+02 3.52385400E+93 8.57548939E+01 -2.96699152E+00	3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.3.
TAJ = 2ATE, 3/ 1/80 0/ 0 0.09000	1.38?18372E+33 MF,MM,ST,DT 30.00000 1+49.00000 3.00000 .15657		A.95787021E+01 DX,DY,DZ,V 6.67417J11E+03 5.52135912E+03 2.36249494E+04 2.51623995E+04	LAT 1.55752436 137.05936197 177.00323	1.80067509E+99 ALPHA 136.01171655 1.54710253 90.74844579 339.99283230	4EV**** 1.00%57 0.00000 0.00000
POSITION AND DISTANCE VELOCITY		VELOCITY RELATIVE TO SUN MAS,X,Y,Z, 4.8536165435E+11 MAG,X,Y,Z, 8.4364025125E+04	1 -4.5855974550E+11 4 -2.7414441144E+04		1.4944733950E+11 -7.9333419283E+04	5.4351299454E+10 -1.3173538067E+04
POSITION AND DISTANCE VELOCITY	POSITION AND VILOGITY RELATIVE TO MOON DISTANCE M16, x, y, 7 VELOGITY M16, x, y, y, 2,7077651,	_4TIVE TO MOON 1.3059152387E+09 2.7077045125E+04	9 .14493893005+0° 4 8.2649533226E+0	·	-3.7236291985E+08 9.1757287582E+03	-2.5920341159E+38 2.445302°135E+04
	2.1743490E-17 1.671691546-07 1.09939553E+02 1.36574948E+12 1.30959852E+12	MEAN ANOM FOCENTRIO II TRUE ANOM PER II NOOL PER II N	2,32173574E+02 2,31431150E+02 2,3068552E+02 8,9508054E+01 8,95505931E+01	AP96EE :: HEISHT :: PERIGE: :: HEISHT :: 0-001 ::	2.6434676.E+03 2.05383863E+02 3.52372594E+03 8.56421563E+001 -2.96701759E+00	13 5 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
0ATE 37 1790 0715 0.00000	4E,44,5T,0T 135,00000 1455,00000	X+Y+2+R -3.00379561E+36 1.10042397E+07 1.79713377E+07	0x,0Y,0Z,V 1.9257435E+04 -1.25543569E+04 1.10870735E+04	LAT; 55.33201791 301.55428529 123.39857	alpha 104.27690665 55.72313314 90.94149709	REV 1.17103 0.00000 0.00999

								06 =
	98E+10	.98E+08			191E+10 159E+04	52E+38 145E+04		8ETA =
0.0000.0	6.4345446698E+10 -2.5713080353E+04	-2.4018452598E+0 1.1917265349E+0		REV 1.34255 0.00000 3.00000	6.4311232991E+10 -5.1219256059E+04	-2.40%2921652E+08 -1.2585153345E+04		4EV 1.35387 0.00000 0.00000
	9 2	-2 1	000000	•	o r	11 50	+ + + + +	•
322,56507473	1.4436718919E+11 -9.7515742327E+04	-5.7344326785E+08 -9.9979933074E+03 F = 3.6374398E	3.63743924E+03 1.99370523E+02 3.51516242E+03 7.60937015E+01 -2.99171164E+00 1.60670127E+00	ALPHA, 344.0933409 51.67364687 90.12927340 213.50256712	1.4827537154E+11 -1.0321805723E+05	-5.8548992475E+08 -1.5691722510E+04 E = 3.6342136E+0	1.95U14442E+U2 3.51946709E+U3 8.1267955F+U1 -2.94906467E+U0 1.80823470E+U0	ALPHA, 338.13025735 45.14505290 69.9999996
55.49583216	1.68	09 -5.73. 04 -9.99	APOGES HEIGHT & PERIGES HEIGHT & U-DOT &	Laf 51.85077194 177.62044531 83.23474 51.85535564	1.48	09 - 5-85 04 - 1-56 APOGEE =	1.1	LAT 45.33747505 171.19733361 91.40345 45.33302399
55.49	36E+11 27E+04	215+ 35E+		51.95 177.62 177.62 51.95	45E+11	1085+09 1745+04 APO	PERIGE PERIGE 0-001 U-001	45.33 171.19 45.33
2.55720933E+04	-4.5857759886E+11 -1.4814127227E+04	1.15919121215+09 2.0846137835E+04 86963381E+02	2.85953341E+U2 2.85U23942E+U2 2.85U37258E+U2 8.95GU25U4E+U1 8.95731505E+U1	1.23204922E+04 -1.83514723E+04 -1.3416752E+04 2.58572052E+04	-4.5859249645E+11 -2.1734637273E+04	9 1.1753775309E+09 4 1.3902590374E+04 3.52044144E+02	3.51914887E+02 3.51784587E+02 8.94273027E+01 8.95468529E+01 8.95747482E+01	0x,0y,0z,V 1.020359446+04 -1.751951136+04 -1.59515650E+04 2.58653532E+04
~	:+11 :+05	60 ÷	N N N 60 60	नम्न	(+11 (+05	60 ± 61	က် ကို ကို ကို ကိ	4440
2.1627472AE+07	TV RE_ATIVE TO SUN Y,2 4.8535207167E+11 Y,2 1.0193105939E+05	2.601043149		x,Y,Z,R 1.27557641E+07 -3.63517938E+05 1.6778520E+07 2.13881535E+07	TY RELATIVE TO SUN Y,7 4.4633355507E+11 Y,2 1.1692609773E+05	3 30 20	TAUE ANOM = TAUE ANOM = KEPL PER = ANOM PER = NOOL PER	x,Y,Z,R 1.339752285+37 -5.618423445+05 1.5159671F+07 2.1384,4627E+07
.16657	VELOSI MAG,X, MAG,X,	VELOCITY MAS: X; Y; MAG; X; Y; 0973779E-	2.17391159E+07 1.70954329E-02 1.10019635E+02 1.35697316E+02 1.354373130E+03	ME.MM.ST.DT 120.00000 1472.00000 1993.00000	VELOGI MAG.X, MAG.X,	VELOGI MAG, K, MAG, X, 1997133	1.5049/15/5-9/2 1.1091712/E+02 1.35659/4/E+92 1.31506319E+02 1.38/54900E+93	МЕ, ММ, ST, DT 121. 93512 1471. 93512 1910.10719
	POSITION AND DISTANCE VELOCITY	DOSITION AND DISTANCE VELOCITY RMO = 6.11		2ATE; 3/ 1/90 0/30 0/30 0.00000	POSITION AND DISTANSE VELOCITY	ITION JISTA VELOG		DATE 3/ 1/90 0/31 50-10718

POSITION AND DISTANCE VELOCITY	VELOGIT MAG, X, Y MAG, X, Y	Y RE_ATIVE TO SUN • 2	1 -4.58695004195+11 5 -2.3949486R1RE+04		1.4826404398E+11 -1.024864566E+05	5.4305551599E+1 -5.?754353163E+0	19E+10 13E+14
POSITION AND OISTANCE VELOCITY	TION AND VELOCITY RELATIVE DISTANCE MAG, X, Y, Z 1. VELOCITY MAS, K, Y, Z 2.	ATIVE TO MOON 1.3385608454E+09 2.4315975465E+04	3 1.177935519E+09 + 1.1784921854E+04		-5.8A18023845E+08 -1.4959072670E+04	-2.4205675637E+0 -1.5119802399E+0	7E+08 19E+04
H OH	4.47020469E-12	440SP =	. 974	+.5	1.60568355E+	2 )	
11 11	2.17403073E+07	MEAN ANOM	2.65265807F-06	APOSER	3.636644496+0	<b>8</b> 0	
	1.63695117E-02	ITRIC =	2.69681085E-06	HEIGHT	1.99548691E+0	20	
11	1.10013589E+02	11	2.74132089E-06	111	3.51950891E+03		
"	1.36655716E+02	PER =	3.94736719E+01		8-14131100E+01		
11	1.31022218F+02	11	8.95454714E+01	= 100-0	-2.98500882E+00	00	
	1.47193512E+03	**	3.95733762E+01	U-00T =	1.80595353E+0	0.0	
OA TE	HE. 44 ST. OT	X.Y.Z.R	0 X • 0 Y • 0 Z • V	LATere	ALP HA	REV	
3/ 1/40	124,17951	1E+07	7.243731936+03	35.64249115	332,26799211	1.39095	HMIN-MAX
95/0		'	-1.52399043E+04	164.74734072	36.45836070	1.00020	
13.77669		_	-1.87825495E+04	80.53158	89.93719500	01.600	
	.16657		2.58649741E+04	36.63826196	205,17776128	00000	
ENA NOTITION	NES OF BYILDS IN THE STATE TO SERVE	ATTVE TO SAN					
DISTANCE		4.8632969923E+11			1.4824971848E+11	5.4297935713E+1	3E+10
VELOSITY		1.1845296305E+05	5 -2.68966724615+04	•	-1.0110749391E+05	-5,5585902510E+0	.0E+04
NOITISON	POSITION AND VELOCITY REL	Y RELATIVE TO MOON					
BUNISIC	ANGE MAG, X, Y, Z	1.3411468424E+09			-5.9019309473E+08	-2.4439960547E+0	7E+0*
	VELOCITY MAG, X, Y, Z	2.4175913103E+04	• 8.8241346016E+03		-1.3578769765E+04	-1.7950565689E+0	19E+04
	5.08247223E-12						
11 •	2-17507125E+07	11	9.56269833€+00	APOGEE =	3.639915445+0	0	
	1.59134032E-02	ITRIC =	9.72549074E+00		2.01844662E+02	20	
81	1.10008950E+02	"	9.89964539E+00	* 1 1	3.51949837E+03	03	
#1	1.36550514E+02	= BER =	8.95345261E+01	HEIGHT =	8-14275942E+01	10	
H ⊃	1.308821035+02	11	8.95432250E+01		-2.97968187E+0	00	
	1.47150130E+03	**	9.95711424E+01	= T0C-U	1.80525015E+0	00	
DATE,	ME, MM, ST, DT	X, Y, Z, R	DX, DY, DZ,V	LAT	ALPHA	REV	
3/ 1/80	6		-5.80836121E+03	00000000	316,66533106	1.50000	DSC NODE
0/43	349		1.52111027E+03	146.77060397	00000000	7.0000°C	
39.23923	2519,23923	-5.53397537E-05 -2	-2.41861658E+04	95.66054	At. 29016325	0000000	
			2.57399840E+04	00000000	199, 3977 2802	0.0000	

5.426439323AE+10 -5.0999776520E+04	-2.5562673181E+08 -2.33532:7775E+04		.23 .03 .03	5.4259380577E+10 -5.3879277307E+04	5951924355E+08 -2.3241403042E+04 3 3 1 1.58342 0.00000
5.4254 -5.0999	-2.5562	+03 +02 +03 +01 +00	REV 1.51528 9.00000 0.00000	5.4259	
1.4819471995E+11 1492207845E+04	-5.9543324104F+08 -3.9580720118E+03	3.646102A2E+02 2.C747355DE+02 3.52.03245E+03 8.24532A40E+01 -2.95691797E+00 1.80122848E+00	aLPHa 314.7696416 -5.19633740 89.23499218	1.4819739985E+11 -9.9778634008E+04	-5.3568399132E+08 -2.2437298700E+03 -2.2437298700E+03 -2.243729870E+03 -2.06849534E+02 -2.06849534E+02 -2.06849534E+02 -2.06849534E+02 -2.06849534E+02 -2.0683913269 -3.08913269 -3.08913269 -3.08913269
		APOSEE = HEIGHT = HEI	LAT, -5.23116530 144.53653353 100.15353		000 1000 000 1000 1000 1000 1000 1000
501735+!! 50764E+!!4	1.1875590468 <u>5+09</u> 4.2320002235+03		<b>≠</b> 4	*9134E+11	<b>ο</b> κ κ
-4.5871750173 <u>E+11</u> -3.9948250764E+!!4	'	4,4534647E+01 4,52444197F+01 4,59625154E+01 8,96805494E+01 8,95413548E+01 8,956339995E+01	0x,0Y,0Y,0 -7,56605055E+03 -4,90705255E+03 -2,40743967E+04 2,57073921E+04	-4.5872079134E+11 -4.1694437713E+04	1.1891459097F+0 4.95923029E+01 4.95923029E+01 5.04572514E+01 8.956239E+01 8.956239E+01 8.95639E+01 0.0507,02,0 -1.31709379E+04 1.39851579E+04 -1.31709379E+04 -1.31709379E+04 -1.31709379E+04 -1.318051579E+04
3E+11 1E+05	.6E+09	சேச்ச <b>்</b> லேல்		3E+11 4E+05	
RFLATIVE TO SUN 2 4.9632675353E+11 2 1.1635544061E+05	RFLAIIVE TO MOON 1.346A917546E+09 2.4061435471E+04	MEAN ANDM ECCENTELS TRUE ANOM KEPL PER ANOM PER	X+Y+2+3 1.51029537E+07 -1.52248597E+17 -1.95028167E+05 2.15336751E+07	VELOSITY RELATIVE TO SUN MAG.x,Y,Z, 4.8632657533E+11 MAG,X,Y,Z, 1.1517837104E+05	2E_ATIVE TO MOON  2.410550722E+04  2.410550722E+04  12
VELOCITY MAG, X, Y, MAG, X, Y,	VELOCITY MAG, X, Y, Z MAG, X, Y, Z	2.174328E+07 2.1744328E+07 1.74434399E-02 1.0993728E+02 1.3656331E+02 1.34037785E+02	4E,444,5T,9T 135,00000 1485,90000 2700,00000		VEL DOITY MAG. x x y x y MAG. x x y x y 373 40 19E - 1 373 572 1E + 1 313 573 1E + 1 35 10 50 00 00 15 31 00 00 00 35 10 00 00 00 15 31 00 00 00 15 31 00 00 00 15 31 00 00 00
POSITION AND DISTANCE VELOCITY	STA		3/ 1/80 3/ 1/80 0/45 0.0000	DOSITION AND DISTANCE VELOCITY	DISTANCE  VELOCITY  A = 1.25  A = 2.17  E = 1.73  U = 1.36  U = 1.36  U = 1.47  TAJ = 1.47

POSITION AND VELOCITY RELATIVE TO SUN

		06=			NODE
049E+10 970E+04	525E+08 525E+04	9ETA =	549E+10 950E+04 718E+08 207E+04		ASC NO
6.4177952049E+1 -2.3342132970E+0	-2.7297727645E+0 1.4263179525E+0 3 2 2 1 1	REV: 1.47155 0.000000 0.000000	6.4174967549E+10 -2.0542504950E+04 -2.6993597718E+08 1.71037271207E+04		REV 2.30300 ASC 99.57322 0.00303 .13357 6.4163822901E+1
1.4805378778E+11 -5.726094886E+04	-5.7147214714E+04 +2 2.0291071781E+04 1 E = 3.64106971E+03 T = 2.0256575F40 E = 3.51324680E+03 T = 7.47436672E+01 = -2.98838247E+00 = 1.80810996E+00	ALPHA, 156.37454562 -42.68121779 89.9999999 332.25626509	1.4904.57531E+11 -5.8207806798E+04 -5.6877061927E+08 1.9345503257F+04	3.641111996+03 2.02519995E+02 3.51590433E+02 7.73123315E+01 -2.98376991E+00 1.80663315E+00	4LPHA, 30 136.7585259 86200000000 944 90.72705931 300 340.00223200
•	000 E	LAT, *** - 42, **7 105779 338, 04059390 202, 51141 -42, 86239431		OGEE IGHT RIGEE IGHT OOT	00000330 15.45732882 177.63344 00000000
2033£+11 4298E+04	50 00 00 00 00 00 00 00 00 00 00 00 00 0	# N 1	5553E+11 5813E+04 1720E+09 53%2=03	- • •	315
-4.59910720335+11 -4.5535004298E+04	9 1.1543906857E+0 4 -1.00270085085+0 1.71389069E+02 A 1.71534593E+02 P 8.94392059E+01 H 8.95384307E+01 U	0X,0Y,0Z,V -9.07935985E+03 1.66753923E+04 1.62672723E+04 2.50025525E+04	-4.5891575553E+11 -4.3091675813E+04 1.1531841720E+09 -7.5171675342=+03	1.800000000E+02 1.80000000E+02 1.80000000E+02 8.94894561E+01 8.958751E+01 8.95661614E+01	DX,DY,DZ,V L 5.12585377E+030 6.04795518E+03 315.4 2.35373708E+04 17 2.51565654E+040
1E+11 4E+04	ស	-	15+11 6E+04 6E+04 6E+09 0E+09	ு என்னிக்கைக் நேர் நேராராரா	<b>ы</b>
4.8635996001E+11 8.4555594514E+04	RELATIVE TO MOON  2.6752596758E+04  4. HEAN ANOM = 1  12. EGGENTRIG = 1  12. KEPL DER = 8  12. KEPL DER = 8  12. NOOL PER = 8	X,Y,Z,R -1,43008539E+07 6,51791050E+06 -1,49981497E+07 2,21238170E+07	PFLATIVE TO SUN 4.85362456315+111 7.3245623426E+04 RELATIVE TO MOON 1.3138495326E+09 7.653331820E+04	HAAN ANOM ECCENTAIC TOUE ANOM ANOM PER NOOL PER	173.15129 -1.5030579547 5 173.15129 1.5030579547 6 1533.07653 -9.01177255E-0; 2 .15657 2.20050304E+07 2 VELOCITY RELATIVE TO SJN
ICE MAG, K, Y, Z	VELOCITY MAS: x, Y, S HAG: X,	ME, MM, ST, DT 157.31472 1517.31472 4538.98291 .16657	445.X.Y.Y. 445.X.Y.Y. 445.X.Y.Y. WELDOITY MAGG X.Y.Y.	665026 743429 7434294 994394 001214 574354 725517	لنا
DISTANCE	DOSITION AND DISTANCE VELOCITY A = 2.5 A = 2.5 T = 1.7 U = 1.3 T A J = 1.3	3/ 1/90 3/ 1/90 1/17 18.89291	POSITION AND DISTANCE VELUCITY POSITION AND DISTANCE VELUCITY	440 E = = = = = = = = = = = = = = = = = = =	34 1780 1729 9.37653 DOSITION AND

CURV AND VELDER ASSESSED						
	ů,	LATIVE TO MOON				
•	445, X, Y, Z	1.3062134959E+0	<b>6</b>		-5.5431621399E+08	
VELOCITY M.S.	24.X4	2.7034293069E+04	4 7.69305541436+03		9.7205358387E+03	2.44743655315+04
840 = 5.5147976	1753F-14					
2.1772	35E+37	,,	2.30604340E+02	AP05EE =	3.64270418E+	0.3
E = 1.6593528	28-B-	EGCENTATO =	2.298773416+02	= THEIGH	2.04640615E+0	20
1,93337	58E+12	"	2.25154170E+02	= is9Iesu	3.52378585E+0	03
= 1.3675	1523E+02	- 23a	8.96675194E+U1		8.57232848E+0	0.1
J = 1.303459306 + 0.2	30E+02	e dia	9.35373230F+01	1 100-0	-2.95775786E+0	00
TAJ = 1.6717131	31 0E+03	"	9.95652579E+01		1.86172547E+0	00
ME, 44	16,75,	5.2.4x	0x, 0y, 0Z, v	LAT,	ALPHA,	9EV,
	0.00000		7.19593984E+03	3.15743389	135.61590662	7.70927
153	000000	1.535702235+07	5.12135441E+03	314.10195122	3.13634155	3.30309
30 543	3.00000		2.35971175E+04	174.92393	30.76577742	0.0000
	.16557		2.517576295+04	3.15641)?3	339.97084466	0.0000
OSITION AND VELSE	SITY REL	COITY RELATIVE TO SUN				
DISTANCE MAS.	7 . Y . X . Z M	4.8535307791E+1	1 -4.59943420318+11		1.4798890663E+11	5.41631513436+10
	- A - A - C + M	A 52707130215405			-7 3866301570F+06	-1 1216776272E+04
	76.6	1. 1. 2. 4. 1. 2. 4. 1. 1. 4. 1. 1. 4. 1. 1. 4. 1. 1. 4. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.			*0.436.7676666	*0.32/32/41/36 ·1.
POSITION AND VELOC	DOITY RE.	LATEVE TO MOON				
CECANOR MACE		1.306167421 RE+09		6	789818115E+08	-2.5310114299E+08
VELOCITY MAG,	2 . X . X . č	2.7071102467E+04	4 8.75274366335+0		7.5941229779E+03	2.4434230557E+04
961	79106-14					
= 2.1772	92F+07	HEAN ANDM	2.34174723E+02	# 3350dV	3.64293729E+	03
E = 1.5555733	01E-02	ECCENTAID =	2.33499007E+02	HEIGHT =	2.04895665E+0	92
= 1.9993	135+02		2-32645039E+02	= 539183d	3.52349144E+	03
1.3675	27E+32	= 23d	8.96663565€+01		8.545481466	0.1
U = 1.3053278	53E+112	11 23d	8.95363387E+01	P-001	-2.95788483E+00	90
TAJ = 1.471573	7315E+03	"	8.955498308+01	U-701 =	1.80176784E+0	0.0
34TE, ME, 44,9	10,12,	5,5.4,x	0X,0Y,0Z,V	1. AT ,	ALPHA,	₹5,0,000
0	135,00000	-2.537754585+16	70	57.24513250	102.	2.17594
1/45 1545.	5.10000			277.21256047		0.0000
0.00000 6300,	0.0000.0	1.814983495+07		121.49145		0.0000
	.15657		2.55853426E+04	57.27916.07	<del>(**</del> *)	0.0000
	0.	_ATIVE TO SUN 4.8535995142E+11			1.4790850779E+11	5.4146956438E+10
VELOCITY MAS+)	Z 4 & 4 X 4	1.0243900209E+05			-4.7905476333E+04	-2.6375505148E+04

CATOCATA OF TOTAL STORY OF THE	7. 3. Lat. VE 10 1007 1. 3163924677E+0	o		-3.5938867507E+08	-2.3540023819E+08
MAS, X,	2.5940359AU0E+04			-1.0336457615E+04	1-1275139350E+94
240 = 4.45113747E-13					
= (.17251756		2.88650101E+02	4P03EE =	3.63613029E+9	.93
1.53031427	E DIGINACCE	2.87727291E+02	# INSIGH	1.9705383654	201
= 1,10019149		2.858 920 T4E+02		3.515207306+03	80
14	c : c	4. 93833585F+01	HETGHT "	7.61304476F	
= 1.35541534	۵ ایا ا	8, 9535 11 04 F + 0.1		-2.992955136+0.0	
1 = 1.47331197		8.95639042E+01		1.409916906+00	.00
10.12.44.34	× . 7 . ×	0x.0Y.0z.v	LAT	ALPHA	9EV.
113.3	1.138400675+37	1.18365345E+04	50,34617505	342,72073821	2.34770
•	-4.670013545+16	-1-81679935+04	153,68624361	50.15697127	0.0000
0000 7203.0	1.547195245+97	-1.40375555E+04	12.75371	90.09452536	0.0000
1.	2.138738915+37	2.58583799E+04	51.14173.52	212, 29171036	0.0000
so AIIDCHEA CHE NCIIISCO	LATIVE TO SUN				
۲.,	4.8534051417E+11	+11 = -4.5437579465E+11		1.4731657194E+11	6.4112193946E+10
43004	1.1737727756+05			-1.0306542533E+05	-5.0954097255E+04
POSITION AND VELOS, IY OF	IY OF LAIIVE TO MOON				
OISTANCE MAGANAY,	1.3372404395+09	60+3254203325+03		-3.7250852783E+08	-2.3537356836E+08
×	2.4397278037E+04			-1.5488918 35E+04	-1.3137627707E+04
RHO = 4.12731279E-12					
= 2,17331333	" MUND NOW	3.54173752F+82	ADOGEF =	3.634079095	¥ 0 ·
= 1.50075+54	# CIGITACCI	3,540352345+02	= IHCIHH	1.959412816+0	5.6
= 1,1331547R		3.539939616+02	* :59125d	3.519557356+87	رق. الم
= 1.35936724	bro	8-942530275+01		8-142854316+01	.0.1
= 1,312,9555		8.953493926+01		-2.98890022E+00	0.0
TAJ = 1.47231348E+03		8.956274376+01	u-22t =	1.809687346+9	.90
7ATS	C47.44X	9x,9y,02,v	LAT,	ALPHA,	3EV
211.	1.398643335407	1.031824928+04	45.51954327	339.45061043	2.36332 BETA = 90
1551.3	-5.577333225+34	-1,753849215+84	149.17594559	45.31914043	σ
71.19332 7231.18002	1,520545345+07	-1.58872573E+04	41.50574	90.000000.06	0.03903
15557	2.138535855+37	2.58535823E+04	45,50503513	209-12356325	0.0000
se Aliuchān cas mollisce	PUS CT BUILD.				
DISTANCE MASSAGET	4.8533917290E+11			1.47808226545+11	5.4107899477E+10
VELOCITY MAGACY Y	1.1755134747E	+05 -2.35349024175+04		-1.0250750293E+05	-5.2703384935E+04

1151446	CE MASAKAY	1.33493755455+39	60+26464441141-1		-5.13744344395+08	-2.37521374415+3	+ J B
V1100.254	44.0	1043614816565			40+31631836864-1-	-1.5347130551F+3	+14
* " C+*	151155	= 650+6	346	٠	4	20	
"	1.97723395F+01					-	
C == 4	2.17397649E+37	# MCNE NABL	3.60000000000		3. 515301774		
"	1.5 255 15 19 19 1- 02		3.590011916+97	HEIGHL #	1.97842905€+02	-5	
- 1	1.133127958+92	E MONE BOAD	3.600034435+02		3.513577358+93	•	
	1.359433435+32	6.30	8.946115375+01		8.151642928+01		
11	1. 309245096+02	CHO NUNE	8.953412345+01	0-101 =	-2.33535538E+00	. 0	
143 = 1	471931346+13		8.956213135+01		1.93772993E+3	•	
JATE,	ME, MM, ST, OF	C, Y, Y, X	V.50.40.XC	LAT	ALPHA	) i o	
	213.71413	1.524193775+07	7.33215374E+03	15.74447547	332.51184408		ANINIMA
27.3	1551,71913	- 7. 739334375+05	-1.523346040+04	142,54527721	46.56055446		
63.19801	7423.08971	27417845F+D7	-1.875115 35E+04	40.62305	89.83705974	0.0000	
	.15657	1,119959195+37	2.545 119 52 5 + 04	35.74364988	205.21205563	0.0000	
CV& NOITISCO	VFL 30	NES CT PATTA SAN					
TOVETOTO	7	4.95171773454	11 -4.52481211245+11		1.47793771575411	5-6100211179F+1	-
					14.0.0000000000000000000000000000000000		
11 Sullan	14 43 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	4 In catatra / t = 1	052.6518557181E+0	. <del>,</del>	-1.01155719856+05	->.>5544?>0457E+0	<b>3</b> D
CVA NOITING		VELOSITY RELATIVE TO MOON					
PERMIT		1.34147623195+			-3.7577115341E+08	-2.398555336E+D	+0.8
VELOCITY		2-4151077633E+04	04 8.8747561422E+03		-1.3554111896E+04	-1.7919871139E+0	30+
5 = C+2	351210						
11	20+326838471.5	II FONT NOW	9.634939315+00	= 335CGV	1.619196175+0		
**	1.671375765-32	H OTATATOR	9.795957855+60	HEIGH	2.01154192F+02		
"	.10007955E+32		9.951239795+00	٠.	3.519559035+0		
**	359454146402	PE 3	B. 95225444E+01		9.15297512F+D		
н	1.30537953E+32	d iid	8.95317655E+01		-2.98046424E+0		
TAU = 1	*56132240E+03		8.9559546%E+01	u-not =	1.806053316+0	0	
04 TE	1C, 18, 44, 31	X,Y,Z,2	0x,08,92,V	LAT	ALPHA	₹.V.	
3/ 1/40	223,22051	95+37	-5.78724855E+03	33300300	316.85152094	2.50003 DSC	C NODE
2/13	1573.22051		-6.63787072E+03	124.50285720	00000000	_	
13.23032	7333.23032	-6.77773105E-04	-2.41849891E+04	95.71932	89.29364733	0.0000	
	.15657	_	2.57383455E+04	00000000	199,99613539	0.00000	
CHE NUITISCA	VELOCITY RE	NUS CT BUILD					
PISTAVOE	Z.Y. X. ZAM EDI	4.853337533E+	11 4.59900115315+11		1.4773858735E+11	5.4055477987E+1	+10
VELOCITY	X O C T M	1.1535917459E+05			-3.1541138536E+34	-5.1003456741E+0	<b>\$0+</b>

1.1535917459E+05 -3.3727149887E+04 -3.1541138536E+34 -5.1003456741E+04

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## APPENDIX C

"REAL WORLD" EPHEMERIS TAPE
AND ITS FORMAT

The real world data tape was generated on Control Data Corporation (CDC) 6000 series machines. It is an unlabeled binary tape written in odd parity at a density of  $556~\mathrm{bpi}$ .

A seven-track non-return-to-zero (change-on-ones) recording scheme is used. Magnetic particles on the tape are aligned in either the positive or negative direction. A binary "1" is recorded by reversing the alignment (polarity); no polarity reversal results in a "0."

A frame of tape data consists of one 6-bit data character and one parity (check) bit for each character. Tracks 0 through 5 specify the characters while track 6 holds the parity bits (see Figure C-1). In binary

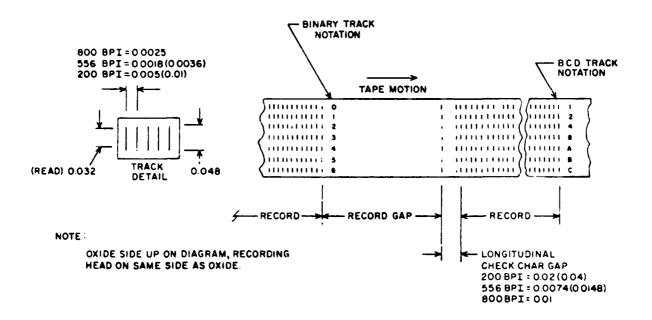


Figure C-1. Bit Assignments on Tape

format, the parity bit is chosen so that the total number of "1" bits in any line is odd. Additional information on the CDC tape processing hardware and procedures is available in CDC Publication No. 60156100.

CDC employs a 60-bit floating point word; its format is shown in Figure C-2. Floating point arithmetic takes advantage of the ability to

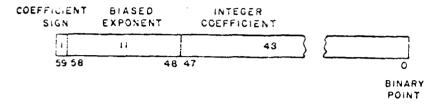


Figure C-2. Floating Point Format

express a number as kB<sup>n</sup>, where k = coefficient, B = base number, and n = exponent. The base number is constant (2) for binary-coded quantities and is not included in the general format. The binary point is considered to be to the right of the coefficient, thereby providing a 48-bit integer coefficient, the equivalent of about 14 decimal digits. The sign of the coefficient is carried in the highest order bit of the packed word. Negative numbers are expressed in one's complement notation. The 11-bit exponent carries a bias of 2<sup>10</sup>(2000<sub>8</sub>) when packed in the floating point word. The CDC procedure used in floating point arithmetic is described in CDC Publication No. 60100000.

The tape contains one file which consists of 216 records. Each record contains 501 words; each word is 60 bits.

The first word in each record is a bookkeeping word; it is an integer quantity equal to the number of data words in that record. Since there are no short records on this tape, this word is always the integer 500. The remaining 500 words are segmented into 50 data frames of 10 words each. Table C-1 gives the ordering and units of the 10 data words.

All position, velocity, and acceleration components are given in an ECI coordinate frame. The X axis of this coordinate system is pointed toward the mean equinox of date at 0 hr GMT of the date of epoch. The X and Y axes form the plane of the true equator at epoch. The Z axis is perpendicular to the true equator at epoch. The set is right handed, with Y lying east of X and Z being positive north.

Table C-1. Data Frame Format

Word	Quantity	Description and Units
i	time	Time, sec from epoch
2	x )	
3	Y	ECI vehicle position, ft
4	$\mathbf{z}$	
5	<b>x</b> }	
6	Ý	ECI vehicle velocity, fps
7	ż	
8	$\ddot{x}_{D}$	
9	$\mathbf{Y}_{\mathbf{D}}$	ECI total atmospheric drag acceleration, ft/sec <sup>2</sup>
10	$\ddot{z}_{D}$	

The data rate on the tape is one data set for each 10 sec. The first time on the tape is 0 sec; it corresponds to the epoch time of 22 hr 30 min 0 sec GMT on 29 February 1980. The last time on the tape is 107990 sec.

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- 3. W. H. Guier and R. R. Newton, "The Earth's Gravity Field as Deduced from the Doppler Tracking of Five Satellites," J. Geophys. Res., 70, 4613-4626 (September 1965).
- 4. R. W. Bruce, An Atmosphere Density Model Recommended for Analysis of Low Altitude Satellite Orbits, TOR-1001(2110-01)-8, The Aerospace Corporation (30 August 1966).
- 5. W. M. Kaula, "Determination of the Earth's Gravitational Field," Rev. of Geoph., 1 (4) (November 1963).